

# 表面等离子喷涂材料研究的现状及发展

中国科学院力学研究所 (北京 100080) 马岳 段祝平 杨治星 吴承康

**[摘要]** 综述了等离子喷涂材料的制备工艺、组织分析和性能测定的研究应用现状。指出了喷涂材料研究应用中仍然存在的问题,也是关键的问题,即涂层与基体的界面结合。针对上述问题,提出了若干的思路以供参考。

**关键词:** 等离子喷涂 喷涂材料 研究现状 发展

在基体材料表面采用等离子喷涂工艺制备涂层,能够大幅度地提高材料的耐磨、抗蚀、抗氧化和热冲击性能,这种工艺广泛用于航空、航天和民用结构部件的处理。因而在工业生产中具有广阔的应用前景<sup>[1~4]</sup>。多年来,本领域广大科研工作者及工程师集中了大量的精力、物力和财力对等离子喷涂涂层的制备工艺、组织和性能进行了一系列的研究。取得了引人瞩目的成果。然而,随着科学技术的发展,对表面喷涂材料的性能要求也不断提高,同时要求涂层材料的制备工艺及设备也不断地改造,涂层材料的组织结构、性能及机理也在逐步深入地研究。本文旨在总结等离子喷涂工艺及材料现状的基础上,为适应科技发展的需要,提出存在的问题、解决的思路和发展的方向,以供参考。

## 1 改善涂层质量及性能的研究

获得高质量、高性能的涂层是涂层制备工艺研究的一个重要课题。普通等离子涂层的内在质量差、与基体的结合强度低,大大地限制了涂层材料的使用及发展。针对存在的问题,国内外进行了广泛的研究,解决的途径可以归纳为三条:

### (1) 调整喷涂过程的工艺参数及改进喷涂设备

据文献[5,6]报道:提高等离子喷涂过程中喷枪的功率,缩短喷涂距离,基体材料预热,采用气道型等离子喷涂工艺制备涂层等措施,能够提高喷涂离子的熔化率,增加离子间和涂层离子-基体间的结合力,减少涂层中的裂纹及孔洞,提高涂层的硬度与内在和表面质量。

### (2) 涂层材料的选择及涂层的前、后处理

文献[7]提出:涂层材料的种类对其性能影响很大。在选择涂层材料时,应遵循:熔融态的涂层材料对

基体具有润湿性;涂层与基体材料的晶体结构匹配,减少界面残余应力和热失配程度;喷涂材料粒子具有热活化作用和高温物化稳定性原则,具备了获得高质量涂层的必要条件。在喷涂前,对基体待喷涂表面进行喷砂、喷丸处理,增加其表面粗糙度,能够提高基体-涂层的结合强度<sup>[7]</sup>。近来,人们又提出了涂层的后处理,包括:对涂层的机械加工和热处理<sup>[7]</sup>,据悉<sup>[3,8]</sup>,涂层的激光重熔处理和 HIP 处理能够大幅度地改善涂层内在及表面的质量。

### (3) 形成梯度复合涂层

由于基体与涂层的材料的化学成分相差较大,使其组织结构和物化性能相差很大,喷涂过程中在基体-涂层的界面处就会由于温变和相变而产生较大的残余应力,降低界面的结合强度,使涂层材料过早失效<sup>[9]</sup>。采用复合的多层涂层<sup>[7,8]</sup>或梯度涂层,能使涂层的化学成分由基体平缓的呈梯度过渡到涂层的表面,减少基体与涂层间的成分差距,致使涂层的组织和物化性能也为连续过渡,避免了基体到涂层的组织、性能的突变,缓解了界面处的应力集中,改善了涂层界面的结合状况,提高了结合强度和涂层的表面硬度,大幅度地改善了涂层材料的性能。

## 2 涂层的微观组织结构分析

通常材料的组织结构决定材料的力学性能,为深入研究涂层材料的使用性能,必须从其组织结构的分析入手。台湾国立大学对等离子涂层组织形貌进行了研究,见图 1。普通等离子涂层中存在较多的孔洞、疏松、微裂纹、密度低,层间为薄弱环节,其相应硬度也很低,通过分析也表明:等离子涂层与基体主要为机械结构<sup>[13]</sup>。

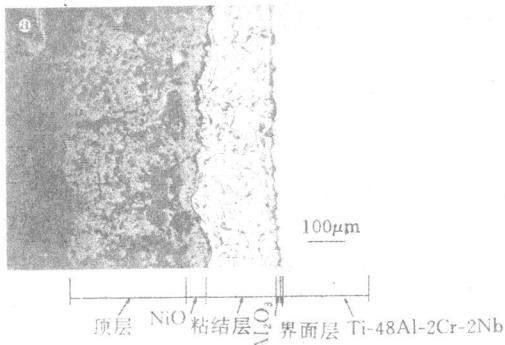


图1 等离子涂层的组织形貌

采用成分为表1的预混粉末制备的涂层用电子探针分析的成分分布见图2<sup>[2]</sup>,从基体-涂层表面Zr元素基本为梯度分布,用SEM分析基体、粘结层到涂层表

面的微观组织表明:从基体到涂层表面氧化锆逐渐增加,粘结剂逐渐减少,涂层明显为层状结构。X射线衍射分析涂层界面由t'-ZrO<sub>2</sub>相和过饱和的Ni基固溶相组成。由此推断,基体-涂层界面的结合主要为机械结合,少部分为化学冶金结合。

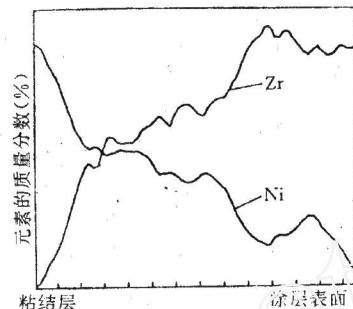


图2 梯度涂层的元素分布

表1 涂层的成分(体积分数 %)

	粘结层	第2层	第3层	第4层	第5层	顶层
厚度/mm	0.2	0.2	0.2	0.2	0.2	0.5
成分(体积分数 %)	100%N	29%Z+N	40%Z+N	60%Z+N	80%Z+N	100%Z

注:N,NiCrCoAlY;Z:体积分数为8%的Y<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>

### 3 涂层性能的测定及研究

通常涂层测定的性能参数有硬度、弹性模量、残余应力、结合强度、热疲劳、抗氧化、耐腐蚀、耐高温、抗热冲击性能。目前较多研究的残余应力、结合强度和硬度等内容、方法及结果主要有如下几个方面。

#### 3.1 残余应力

目前测定上述性能的方法还没有形成一个非常统一的标准,各研究者所用方法不一,有些是直接用现成的仪器及设备,有些是测定其间接的参数,反映其性能的指标,归纳起来大致有以下几种<sup>[14,15]</sup>:

(1) 对涂层进行热循环处理,用XRD测定和评价残余应力、相及晶格参数。

$$\sigma = E_d \alpha_d \Delta T$$

式中:E<sub>d</sub>为弹性模量,α<sub>d</sub>为体积膨胀系数,ΔT为弹性粒子与基体间的温度差。

采用标准的Bragg定律、反射倾角法,此方法只能适用于XRA能穿透的涂层厚度。

(2) 钻孔法,只适用于厚度大于0.3mm的涂层。

(3) 悬臂梁法,适用于较薄的涂层。

#### 3.2 微观硬度

由EPMA测定的梯度涂层的元素的分布呈连续的分布,从相上有一个从t-m的转变。在氧化锆热障涂层中氧化锆含量增加,密度减小。微观硬度在涂层中的分布见图3a和图3b,表明多层复合层的成分、密度及硬度呈连续分布。

#### 3.3 结合强度

表面喷涂材料在承受各种载荷时,破坏通常发生在涂层与基体的界面处,涂层与基体的界面结合强度是决定材料整体强度的关键因素,也是评价涂层质量最关键的指标。但界面结合强度的测定方法还是一个未严格规范化、系统化和完善的问题。目前,各国都制定了涂层-基体间结合强度试验的相应标准,例如,ASTM C633-79、JIS-H8664、GB/T13222-91、GB8641-88、GB8642-88和GB12305.5-90等。归纳起来,有关涂层-基体界面结合强度的测定有几种方法:

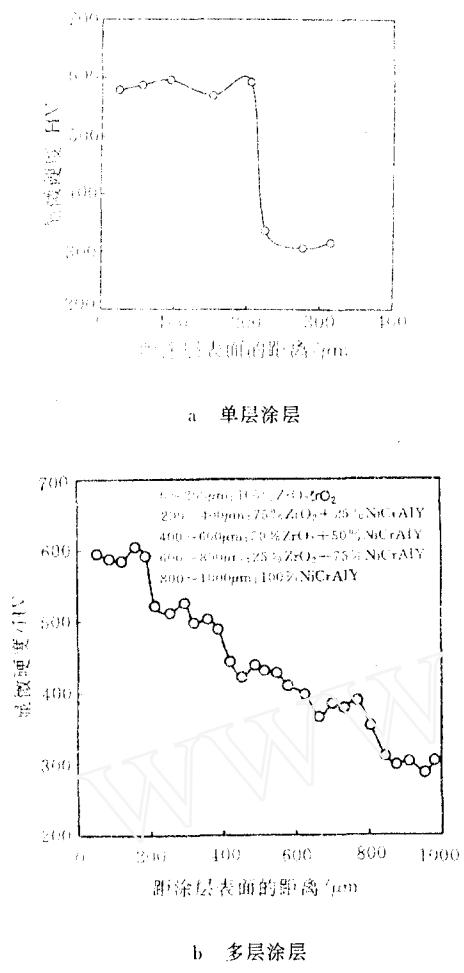


图3 涂层的显微硬度分布

(1) 超声波测定法<sup>[17,18]</sup> 是一种非破坏性的检测方法。它是利用超声反射波在涂层试样中的反射强度或超声波在试样中的传播速度来评价结合强度。反射强度越高,表明结合强度越高。用这种方法研究陶瓷涂层结合强度与涂层性能之间的关系,结果为:涂层的密度、显微硬度增加、孔隙率降低<sup>[19]</sup>。

(2) 粘强拉伸法<sup>[20]</sup> 此方法有标准 GB12305.5—90。它是将涂层试样与配副试样用胶粘结起来,在拉伸试验机上进行拉伸,涂层被拉脱时的载荷与涂层面积之比为结合强度。

(3) 界面压入法<sup>[21]</sup> 在等离子喷涂层与基体界面上,用一定的载荷或不同固定的载荷作用在维氏压头上,使界面开裂。用裂纹的长度或有关的参量来表征结合强度。

(4) 悬臂梁法和三点弯曲法<sup>[22~24]</sup> 通过测定临

界应变能释放率、极限应力强度因子,反映涂层与基体的结合强度。

采用 ASTM C633—79 标准拉伸法测定的粘结强度与涂层层数和涂层厚度的关系见图 4、图 5,可以看出:涂层的层数越多,结合强度越高;涂层越厚,结合强度越低;涂层经过热处理其结合强度增加,HIP 处理比普通热处理的效果更明显<sup>[11]</sup>。

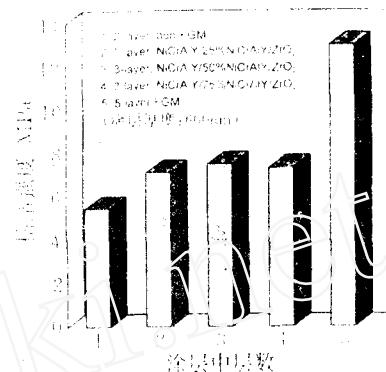


图4 涂层层数对粘结强度的影响

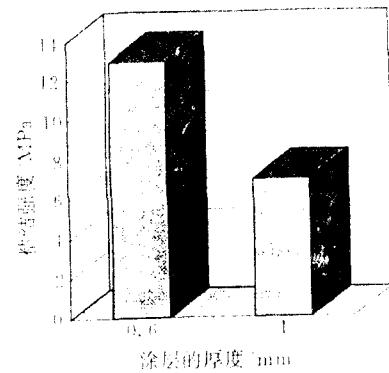


图5 涂层厚度对粘结强度的影响

#### 4 等离子喷涂材料的发展

在表面等离子喷涂材料中,涂层与基体的界面是一个很重要、也很棘手的问题,通常喷涂材料的整体强度主要决定于界面的结合强度,就目前的研究来看还没有从根本上解决界面结合的问题。以陶瓷涂层金属基体为例,陶瓷与基体的性能和组织相差都很大,两者结合必会形成明显的界面,该处物化性能和组织结构

突变成为残余应力和缺陷的聚集处,材料承载时破坏发生在界面。解决这类问题的思路是:①研究新界面层材料,使其性能和组织结构既接近涂层又接近基体,加在基体与涂层间起过渡和搭桥的作用。②基体待喷表面改性处理,使其组织结构接近基体。③发展新工艺,在基体-涂层的界面处形成梯度分布,消除明显界面,使组织和性能呈连续的分布。总的目的是采取措施,提高界面的结合强度。

### 参 考 文 献

- 1 Gu Y W et al. Functionally graded  $ZrO_2$ -NiCrAlY coatings prepared by plasma spraying pre-mixed, spheroidized powders. Surface & Coating Technology, 1997, 96: 305~312
- 2 Xiang Xinhua et al. Fabrication and microstructure of  $ZrO_2$ /NiCrAlY graded coating by plasma spraying. Surface & Coating Technology, 1996, 88: 66~69
- 3 Pei Y T et al. Laser cladding of  $ZrO_2$ -(Ni alloy) composite coating. Surface & Coating Technology, 1996, 81: 131~135
- 4 刘正林等.  $ZrO_2$ 隔热梯度涂层制备技术及其性能研究. 表面技术, 1997, 26(4): 4~7
- 5 Akira Kobayashi. Formation of high hardness zirconia coatings by gas tunnel type plasma spraying. Surface & Coating Technology, 1997, 90: 197~202
- 6 Kobayashi A et al. J. High Temp. Soc. 1992, 18: 89
- 7 李应有等. 涂层材料设计初探. 表面技术, 1997, 26(4): 24~27
- 8 Liang G Y, Wong T T. Microstructure and character of laser remelting of plasma sprayed coating (Ni-Cr-B-Si)on Al-Si alloy. Surface & Coating Technology, 1997, 89: 121~126
- 9 Xianting Zeng et al. Development of graded Cr-Ti-N coat- ings. Surface & Coating Technology, 1998, 102: 108~112
- 10 Helemersson U et al. J. Appl. Phys., 1987, 62: 481
- 11 Sundgren J E et al. Thin Solid Films, 1990, 193/194: 818
- 12 Holleck H, Schulz H. Thin Solid Films, 1987, 153: 11
- 13 Hsu I C, Wu S K. Oxidation improvement of Ti-48Al-2Al-2Cr-2Nb intermetallics by air plasma sprayed  $ZrO_2$ -Ni-4.5% (质量分数) Al coatings. Surface & Coating Technology, 1997, 90: 6~13
- 14 Anthony J Perry et al. Practical measurement of the residual stress in coating. Surface & Coating Technology, 1996, 81: 17~28
- 15 Hamacha R et al. Residual stress evolution during the thermal cycling of plasma-sprayed zirconia coatings. Surface & Coating Technology, 1996, 80: 295~302
- 16 Li Jun et al. Electroforming of nickel and partially stabilized zirconia(Ni+PSZ)gradient coating. Surface & Coating Technology, 1997, 91: 131~135
- 17 Suga Y. Proceedings of 13th ITSC, USA, 1992: 247~252
- 18 Nambu Y. Proceedings of 13th ITSC, USA, 1992: 241~246
- 19 Kawase R. Proceedings of 4th National Thermal Spray Conference, USA, 1991: 187~191
- 20 Matsubara Y. Proceedings of 13th ITSC, USA, 1992: 637~641
- 21 Choulier D. Proceedings of 6th International Conference on Heat Treatment of material, USA, 1988: 75~78
- 22 Mcpherson R. Thin solid Films, 1981, 81: 297~310
- 23 Schweitzer K K. Surface and Coating Technology, 1991, 48: 103~111
- 24 Guo D. Surface and Coating Technology, 1993, 57: 175~184

(收稿日期:1999-05-04)

## 漆包线退漆新法

由于漆包线铜的含铜量非常高,有时在装联工艺中多利用废旧的漆包线镀银作各种联接导线的作用,具有良好的电性能稳定效果。

漆包线镀银前必须把漆膜退除,以往我们采用在热碱溶液中煮或在退漆剂中退除,但这两种方法实际效果不太理想。

我们改用在浓硫酸中退除办法效果很好,具体操作步骤如下:

第一工序:在工业级浓硫酸(98%)中浸3~5s。

第二工序:在铬酸液中漂洗黑膜, $CrO_3$ :150~200g/L,漂洗时间5~10s。

经铬酸液漂洗之后再经两道水洗之后,即可镀银,质量得到保证的同时大大简化了工艺过程。

胡光军 (蚌埠市职工技协站)

## MAIN ABSTRACTS

### The Development and Status in Investigation on Surface Plasma Spraying Coating Material

The summary has been conducted on the investigation and application status of preparation technology, analysis structure and measure properties in plasma spraying coating material. It is pointed out that the improvement of cohesion properties of interface between coatings and substrate is a key in the research and application of plasma spraying material. A lot of ideas to improve cohesion properties are put forward for providing reference.

**Keywords:** Plasma spraying material Investigation status Development

### A Study of Pitting Corrosion Defect on the Surface of 6063 Aluminum Extrusion

By means of SEM, EPMA, corrosion morphology and corrosion products occurred on the surface of 6063 aluminum extrusion was examined. The results demonstrated that snowflake corrosion defect was composed of dense pittings, and that in fact, this corrosion was a pitting corrosion. The cause of corrosion was attributed to the segregation of anodic particle Mg<sub>2</sub>Si in the alloy. It was also found in the experiments that the pH value and the Cl<sup>-</sup> concentration in rinse water after dismutting were key factors to the occurrence of pitting corrosion defect.

**Keywords:** 6063 aluminum extrusion Pitting corrosion Anodizing

### Study on Structure and Performance of Lumpish or Granular Borided Layer

The borided layer of low temperature is usually tooth-like, and its structure is even, fine and close, short of porosity and black spots. Adding too much halogenide and thiocetazone into the boriding agent, lumpish or granular structure full of porosity and black spots is found. According to the results of microscope, EPMA and X-ray diffraction, the lumpish or granular structure is still borided layer. The difference between tooth-like borided layer and lumpish or granular borided layer by means of wear comparison test and measurement of anode polarization is discussed. That is, wear resistance of tooth-like borided layer is superior to that of lumpish or granular borided layer, but corrosion resistance of tooth-like borided layer is much inferior to that of lumpish or granular borided layer. The simple explanation is expounded in the paper about it.

**Keywords:** Structure Performance Lumpish or granular borided layer

### Study on the Technology of Chemistry Plating TL-6-2 Ni-P Alloy

Study on the rational prescription and the technology of plating through the experiment. The plating solution is easy to plate and readjust. The employing life-span can reach six cycle. The deposit of plating is compact, bright and clean. The test of acidproof the dense nitric acid last more than 3 minutes; The deposits are wear-resistance and antifriction and high hardness. The hardness can reach more than HV1000 through the harden treatment. It's fit to apply in industry for the material is from the industrial raw material.

**Keywords:** Chemical plating Ni-P alloy Stain resistance

### Study on Polyester-Acrylic Paint

Polyester paints and acrylic paints take great proportion on the advanced automobile coatings. In order to utilizing individual advantages, Polyester and acrylic polymer have been polymerized with some functional groups. My exploratory research works are described in this paper.

**Keywords:** Coatings Polyester resin Acrylic acid

### Research of KCl Zn-plating improving corrosion resistance and discolorment resistance

Having reached the corrosion-resistance and discolorment-resistance principle of KCl Zn-plating low-Cr color or passivation, at the same time using the way to dosing the passivated Zn-coating with coupling agent to improve the corrosion resistance and discolorment resistance. During the closing and drying process, silane coupling agent absorbed on the closed surface more to the gap in the frame which is formed with the Cr<sup>3+</sup> compound of the passivated coating, and is dissociated into Si-alcohol groups, then the Si-alcohol group form the hydro-bond with OH-group on the passivated coating or bond SiO-M (M is an inorganic surface). Meanwhile, silicon alcohol group in each molecule of silane coupling agent condensates each other, and forms membrane fillings of net construction or covering at passivated membrane surface, which produces a new construction and improves corrosion-resistance.

**Keywords:** Zn-plating Closing Discolorment Corrosion-resistance