Available online at www.sciencedirect.com

ScienceDirect

Procedia Engineering 67 (2013) 147 – 154

Procedia Engineering

www.elsevier.com/locate/procedia

7th Asian-Pacific Conference on Aerospace Technology and Science, 7th APCATS 2013

Study on Judgment Method of Combustion Mode on dual-mode Scramjet

Q. Chen[a], L. H. Chen[a], H. B.Gu[a], X. Y.Zhang[a], P. Wang[b,*]

[a]*State Key Laboratory of High-Temperature Gas Dynamics, Institute of mechanics, Chinese academy of sciences, Beijing, 100190, China*
[b]*China University of Petroleum, Beijing, 102249, China*

Abstract

It was very significant to judge the combustion mode of engine correctly, because the distributions of fuels and other parameters of combustion mode switching depended on it. This paper proposed to a judgment method of combustion mode of engine, namely artificial neural network method, based on the dual-mode scramjet experiments and analysis results. It made use of experimental measurement values, and the parameters along engine were obtained through one dimensional analysis. This method provided the basis for the combustion mode design of engine in the future.

Selection and peer-review under responsibility of the National Chiao Tung University

Keywords: Combustion mode, Scramjet, Artificial neural network

Nomenclature

A	area
C_f	skin friction coefficient
C_{fuel}	coefficientof fuel distribution
c_p	specific heat at constant pressure
h	specific enthalpy
M	Mach number
p	static pressure
R_{Ac}	area ratio of combustor outlet to inlet
T	statictemperature

* Corresponding author. Tel.: +86-10-89731770.
*E-mail address:*wangpei@amss.ac.cn

Selection and peer-review under responsibility of the National Chiao Tung University
doi:10.1016/j.proeng.2013.12.014

V	velocity
$X_{H_2O,vit}$	mole fraction of water vapor in the vitiator products
x	position in x-direction
Y	mass fraction
Greek symbols	
γ	ratio of specific heat
η	combustionefficiency
η_{sto}	stoichiometric combustion efficiency
ρ	density
ϕ	stoichiometric ratio
Subscripts	
i	component

1. Introduction

In the range of flight altitude 18~30 km and fight Mach number 4~7, the dual-mode scramjet with hydrocarbon fuels is one of the most competitive air breathing propulsion systems [1, 2]. In order to maintain the high performance of engine in the range of flight altitude and Mach number, the combustion mode in combustor is necessary to be switched [3]. In general, at lower flight altitude and Mach number, an engine with subsonic combustion mode attains higher performance than an engine with supersonic combustion mode. On the contrary, a supersonic combustion mode engine has the higher performance at higher altitude and Mach number. It was very significant to judge the combustion mode of engine correctly, because the distributions of fuels and other parameters of next combustion mode switching depended on it.

With the drastic development of computer technology, the artificial neural network method had made great applications in many fields, such as high performance aircraft autopilots, flight path simulations, aircraft component fault detectors [4]. One of the most important applications was pattern recognition technology. A neural network was able to learn to recognize the pattern from the observed data or experiment data. That was a novel method to judge the combustion mode of dual-mode Scramjet engine.

Based on the dual-mode scramjet experiments and analysis results, this article proposed to a judgment method of combustion mode of engine, namely artificial neural network method. It made use of experimental measurement values, such as burned and unburned pressure distributions, fuel injection positions, and fuel equivalence ratios. The parameters along engine were obtained through one dimensional analysis. Then they were treated as learning cases of the neural network. After being trained by the learning cases, the judgment model was established, providing the basis for the combustion mode design of engine in the future.

2. Experimental Setup and Analysis Method

2.1. Experimental Setup

The experiments applied to the paper were performed on the direct-connected facility which was specially designed for dual-mode scramjet combustor experiments. The experimental gas was heated by a vitiator, which burned hydrogen and replenished oxygen to maintain oxygen mole percentage at 21% in the experimental gas. There were two types of condition at the entrance of isolator. The details of the flow parameters were shown in

Table 1.

Table 1Operation parameters of facility

Mach number	Total temperature(K)	Total pressure (MPa)	Mass ratio(kg/s)
1.8	950	0.6	1.8
2.5	1650	1.0	1.2

There were also three types of test models, which were named as Model-1, Model-2, and Model-3 to perform experiments. The schematics of the test models were shown in Fig.1. The test model consisted of isolator, combustor and nozzle. Three models had the same isolator. The differences of the models were the expansion angels of the combustor. The combustor of Model-1 had three expansion sections with angles of 1.5°, 2.0° and 3°. However, Model-2 and Model-3 only had two expansion sections and the angles were 1.5°, 2° and 1.5°, 3° respectively. The fuel C_2H_4 was injected into and burned in a cavity-based flame holder. The positions of fuel jet were shown in Fig.1.

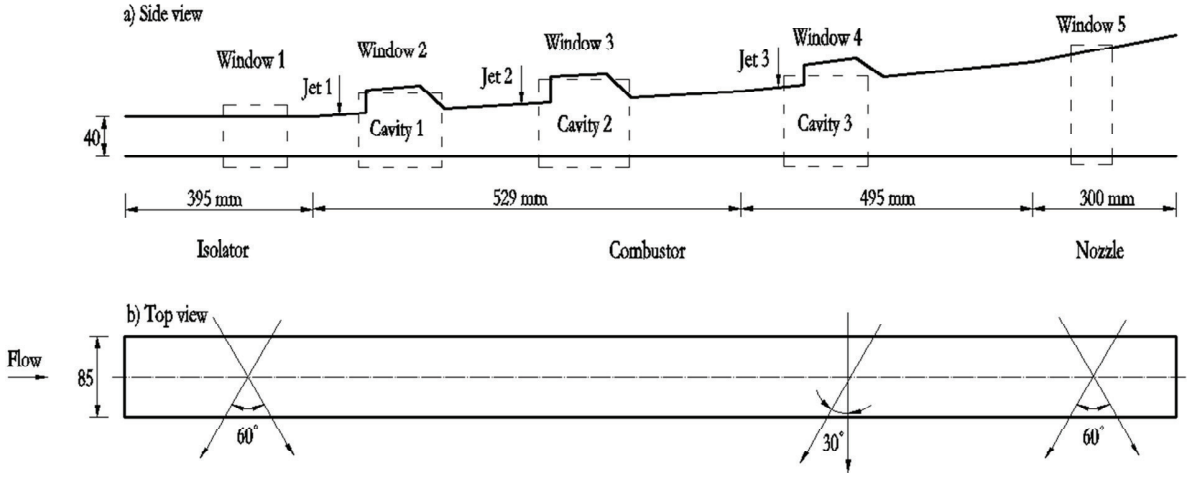

Fig.1Schematic of direct-connected scramjet test facility

2.2. Quasi 1-D AnalyticalMethod

In order to analyze the experimental data deeply, this paper developed a quasi-1-D analytical model based on the experimental data. One step chemical reaction was assumed that includes only the major species of C_2H_4, H_2O, CO_2, O_2, and N_2.The chemical equation was shown in Equ.(1)where ϕ and η respectively representedstoichiometric ratioand combustion efficiency. $X_{H_2O,vit}$ wasthe mole fraction of water vapor in the vitiator products.

$$\phi C_2H_4 + 3\left(O_2 + \frac{X_{H_2O,vit}}{0.21}H_2O + \left(3.76 - \frac{X_{H_2O,vit}}{0.21}\right)N_2\right) = (1-\eta)\phi\, C_2H_4 + 3(1-\phi\eta)\, O_2 + \left(2\phi\eta + 3\frac{X_{H_2O,vit}}{0.21}\right) H_2O + 2\phi\eta\, CO_2 + 3\left(3.76 - \frac{X_{H_2O,vit}}{0.21}\right)N_2 \quad (1)$$

Equ.(2)~(5) were the governing equations of the analyticalmethod. They were mass, momentum, energy conservation equations and state equation. Assuming that the combustor wall was adiabatic, the term of convective heat transfer did not exist in Equ.(3).

$$\frac{\mathrm{d}\rho}{\mathrm{d}x} = -\frac{\rho}{V}\frac{\mathrm{d}V}{\mathrm{d}x} - \frac{\rho}{A}\frac{\mathrm{d}A}{\mathrm{d}x} \tag{2}$$

$$\frac{\mathrm{d}V}{\mathrm{d}x} = -\frac{V}{\gamma M^2}\left(\frac{1}{p}\frac{\mathrm{d}p}{\mathrm{d}x} + 2\frac{\gamma M^2 C_f}{D}\right) \tag{3}$$

$$\frac{\mathrm{d}T}{\mathrm{d}x} = -\frac{1}{c_p}\left(\sum_i h_i \frac{\mathrm{d}Y_i}{\mathrm{d}x} + V\frac{\mathrm{d}V}{\mathrm{d}x}\right) \tag{4}$$

$$\frac{1}{\rho}\frac{\mathrm{d}\rho}{\mathrm{d}x} + \frac{1}{T}\frac{\mathrm{d}T}{x} - \frac{1}{p}\frac{\mathrm{d}p}{\mathrm{d}x} = 0 \tag{5}$$

The skin friction coefficient C_f in Equ.(3)was determined using the method given by JAXA [5]where:

$$C_f = \frac{0.38\left(1+\frac{\gamma-1}{2}M^2\right)^{-0.467}}{\left(\log \mathrm{Re}_x\right)^{2.58}} \tag{6}$$

For the governing equations,a continuous wall pressure distribution $p(x)$ wasneeded to solve the equations system. This distribution function could be obtained from the discrete experimental data by creating 3-peak Gaussian fits. The Gaussian peaks were encountered in many areas of science and engineering, and was given by

$$p = \sum_{i=1}^{3} a_i \exp\left[-\left(\frac{x-b_i}{c_i}\right)^2\right]$$

Where a , b , c wererespectivelythe amplitude, the centroid (location) and the peak width. The engineering enthalpy of each species was a function of the temperature $\left(h_i(T)\right)$ [6]. These values were obtained at a given temperature from the tabulated thermodynamic data in the Burcat's report. Y_i was the mass fraction of species i, and the term $\mathrm{d}Y_i/\mathrm{d}x$ could be written as the function of $\mathrm{d}\eta/\mathrm{d}x$. Because the mole quantities did not change during the processing of C_2H_4 combustion, the average molecular weight did not change. So, the state equation could be written as Equ.(5).

In the system of equations, there were nine unknownvariables which were ρ, V, T, η, Y_i .And there were also nine differential equationsincluding four equations of $\mathrm{d}Y_i/\mathrm{d}x$ and $\mathrm{d}\eta/\mathrm{d}x$. So, the equations system could be integrated through the numerical method.

2.3. Radial Basis Function（RBF）neural network

RBFneural network (Fig.2) was a feed forward network with three layers based on regularization theory. A Gaussian RBF monotonically decreased with distance from the center (Fig.2(b)). So,Gaussian-like RBFs were local (give a significant response only in a neighborhood near the response only in a neighborhood near the center) and are more commonly used than multiquadric-type RBFs which have a global response. They are also more biologically plausible because their response is finite.

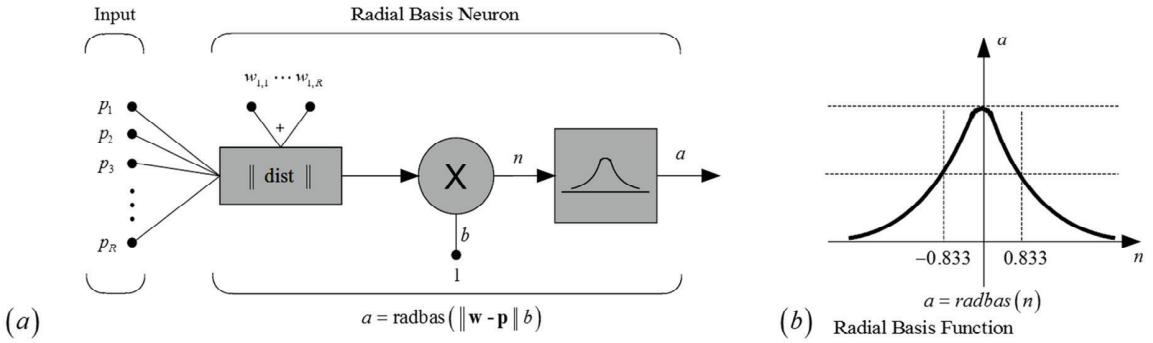

Fig.2Architecture of RBF neural networks,(a) Radial basis neuron,(b) Radial basis function

At present, the RBF Neural network can deal well withthe problem including classification and pattern discrimination.The problem of Scramjet combustion modes diagnose belonged to the category. RBF Neural network required a supervised learning the existing classification results,then the network would update the weights of neurons. After the learning processing was completed, the network would be able to classify the new inputs.

In this paper, considering the characteristics of scramjet combustion parameters, the inputs of RBF network in this problem were listed in Table 2. R_{Ac} represented the extend of combustor expansion, C_{fuel} represented the conditions of fuel distribution, and the bigger the value was, the distribution of fuel was near to the combustor outlet. η_{sto} represented the relative quantities of heat release.

Table 2 Inputs of RBF network

Input	Expression	Range of input	Clarification
$M_{iso,in}$	-	1.8, 2.5	Mach number at outlet of isolator
R_{Ac}	$A_{combustor,out} / A_{combutor,in}$	1.8525, 1.895, 1.9825	Area ratio of combustor outlet to inlet
C_{fuel}	$\sum(\phi_i/\phi)\cdot(x_{fuel\_jet\_i}/L_{combustor})$	0.55~0.86	Coefficient of fuel distribution
η_{sto}	$\eta\cdot\phi$	0.12~0.55	Stoichiometric combustion efficiency

3. Results and Discussion

3.1. Analysis of the experimental results

There had been 30 experiments withdifferent conditionsfor three types of engine models, which were carried out at the direct-connected scramjet test facility. Among the experiments, there were 14 times of experiments whose condition of the entrance was Mach number 1.8, and other experiments were Mach number 2.5.The fuel equivalence ratio was between 0.3 and 0.8 at these experiments. In Fig.3, two typical experimental parameters distributions were shown. The blue dotsshowed in the illustrations represented the experimental pressure distributions along the combustor. The black lines at the bottom of the figure depicted the inner passage of the combustor. The Mach number at the entrance was 2.5 in Fig.3(a), 1.5 in Fig.3(b).And the other detailed flow parameters at entrance were shown in Table 2 and Table 3. In experiment (a) the fuel C_2H_4 was injected into the combustor at two different positions and the total equivalent ratio was 0.38. In experiment (b), the fuel C_2H_4 was

injected into the combustor at 4 positions and the equivalent ratio was 056.At the aspectof the distribution parameter of fuel C_{fuel} , the fuel layout of the experiment (a) was front of experiment (b) relatively.

Applyingthe quasi-one-dimensionanalyticalmethod mentioned in section 2.1, the distributions of parameters could be obtained in the combustor. The distributions of Mach number (green lines), static pressure P (blue lines), and combustion efficiency (red lines) were shown in Fig.3. The figure showed that the trend of static pressure distribution measured by experiments was well fitted through the method of Gaussian fitting. Experiment (a) was at supersonic combustion mode, because the Mach number was is greater than 1in the combustor. However, for experiment (b), Mach number was under 1 in some region, though the flow returned to supersonic flow at back of combustor. So, experiment (b) would be judged as the subsonic combustion mode. At the aspectof combustion efficiency, the combustion of supersonic mode was relatively severer than subsonic mode, because combustion efficiency curve of supersonic mode rose rapidlyat the shorter region. However, the efficiency curve ofsubsonic combustion modewas more uniform in combustor.

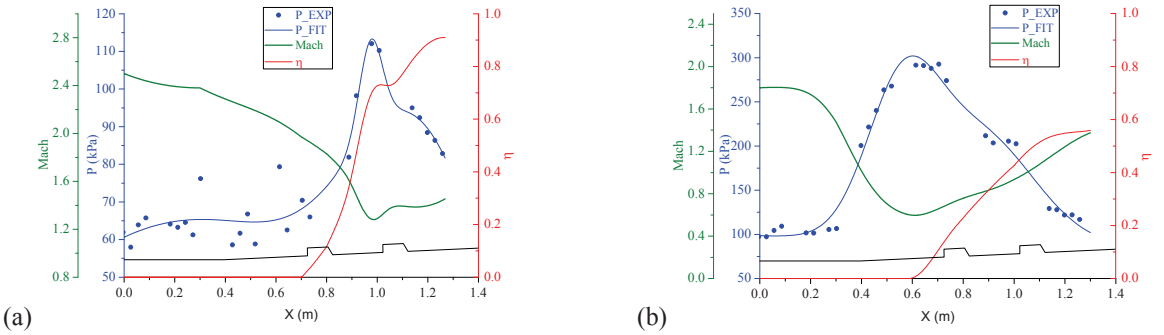

Fig.3 Distributions of flow parametersin the combustor for (a)supersonic combustion mode and (b)subsonic combustion mode

Table 3 Parameters of experiment (a) and (b)

Input	(a)	(b)
$M_{iso,in}$	2.5	1.8
R_{Ac}	1.982	1.895
C_{fuel}	0.77	0.81
η_{sto}	0.35	0.32

3.2. RBFneural networkmodeling

Depending onMach number distribution along the engine, the combustion mode of the experiment could be judged.For 30 experiments under different working conditions, the distributions of Mach number could be obtained through the method introduced in section 2.1. Then the RBFneural network model for combustion mode determiningcould be established according to the method from section 2.2. The RBF neural network's inputscontainedfour groups of parameters were shown in Table 2.

In order to verify the robustness of the network, the 25 samples were randomly selected from 30 experiments as the training set. And the five rest samples (twoexperiments of supersonic combustion mode and three experiments of subsonic combustion mode) were used as the test set, to verify the judgment ability of the network.

The neural network of mode determining wasconsisted of 25 neurons and divided into two layers. By learning from samples, the neuron weight matrix wasupdated. For the five test samples, the network had predicted the combustion mode rightly. Namely, the RBF neural network had good adaptability to the problemsof combustion mode classification.

3.3. The parameters analysis of engine combustion mode

The parameter analysis of combustion mode was carried out in this paper through RBF neural network model.The supercritical curveof supersonic/subsonic combustion mode was obtained when some parameters was fixed. Fig.4 showed the combined effects of the coefficient of fuel distribution C_{fuel} and stoichiometric combustion efficiency η_{sto} on combustion mode when M_{iso_in} and R_{Ac} were fixed.

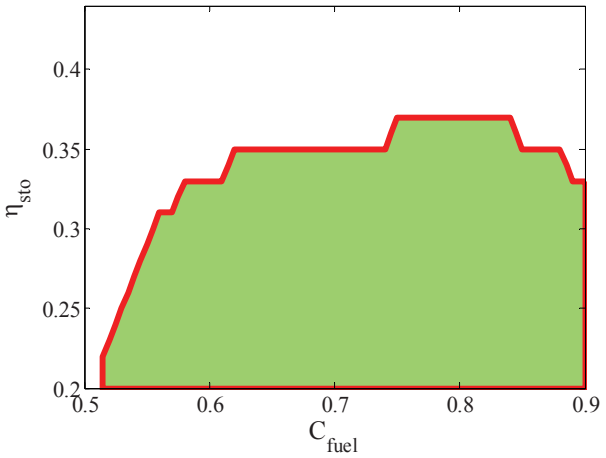

Fig.4 Effects of C_{fuel} and η_{sto} onthe combustion mode

Fig.4 showed when the situations were in the green range,the scramjet was at supersonic combustion mode. Butat other regions the scramjet was at subsonic combustion or unstarted mode. It also could be known when C_{fuel} is smaller than 0.65 (fuel was mainly injected at the forward section of combustor), the engine mode was affected by the combined influences of C_{fuel} and η_{sto}. The engine could not maintain the supersonic modeunless the fuel mainly released heat at back of combustor when η_{sto} rose. When C_{fuel} was greater than 0.65, the relationship between mode and fuel distribution coefficient of the engine was no longer significant. In addition, when η_{sto} was greater than 0.35, the engine could not maintain supersonic mode no matter how the fuel distribution in the combustor. The engine would turn into the subsonic or unstarted mode.

4. Conclusions

In this paperthe combustion mode of dual-mode scramjet judgment method was developed.Direct-connected experimental results of three scramjet combustor models and two entrance situations were analyzed by a one-dimensional method.The important parameterswere obtained, such as C_{fuel}, η_{sto} and the combustion mode. Then the judgment model based on the RBF neural network was built by learning the obtained combustion mode. The followings werethe conclusions:

(1) One-dimensional analysis methodwas able to calculate the flow parameters of the engine combustor effectively.

(2) RBF neural network models could be applied to judgethe engine combustion mode, and the accuracy of judgment was acceptable.

(3) Under the inner geometryand entrance conditions unchanged, the combustion mode was affectedby C_{fuel} and η_{sto} when η_{sto} was relatively small. However, when η_{sto} was larger, the combustion modewas less affected by C_{fuel}.

Acknowledgements

The project is partially supported by the State Key Laboratory of High-Temperature Gas DynamicsFoundationand China University of PetroleumFoundation (KYJJ2012-06-07)

References

[1] E. T. Curran, F. D. Stull, 1964. "The utilization of supersonic combustion ramjet systems at low machnumbers", Aero Propulsion Laboratory, RTD-TDR-63-4097.
[2] F. Billig,1988. Combustion processes in supersonic flow, Journal of Propulsion and Power, 4(3),209-216.
[3] S. Tomioka, K. Tani, R. Masumoto, S. Ueda, 2009. "Dual-mode operation of a rocket-ramjet combinedcycle engine", 27th International Symposium on Space Technology and Science, Tsukuba(Japan), ISTS Paper 2009-a-26.
[4] Hagan, Martin T., Howard B. Demuth, and Mark H. Beale, 1996. Neural Network Design, 1st ed. 1 vols Boston: PWS Pub.
[5] Mitani, T., Hiraiwa, T., Tarukawa, et al, 2002. Drag and total pressure distributions in scramjet engines at Mach 8 flight, Journal of Propulsion and Power, 18(4): p. 953-960.
[6] Alexander Burcat and BrankoRuscic,2005. "Third Millennium Ideal Gas and Condensed PhaseThermochemical Database for Combustionwith Updates from Active Thermochemical Tables", Argonne National Laboratory Report, ANL-05/20 TAE 960.