



A high performance fifth-order multistep WENO scheme

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Summary

Many efforts have been made to improve the accuracy of the conventional weighted essentially nonoscillatory (WENO) scheme at transition points (connecting a smooth region and a discontinuity point). This paper analyzes these works and further develops a more effective multistep WENO scheme. Theoretical analysis and numerical results show that the new scheme not only improves the accuracy by one order higher than the traditional fifth-order WENO schemes at transition point but also maintains the fifth-order accuracy in smooth regions even at critical point where the first derivative vanishes.

KEYWORDS

critical point, high performance, low-dissipation, multistep WENO scheme, transition point

1 | INTRODUCTION

The weighted essentially nonoscillatory (WENO) schemes have been extensively studied and applied in computational fluid dynamics since it was first proposed by Liu et al.¹ The distinctive advantage of the WENO scheme is that it not only can achieve uniform high-order accuracy in the smooth areas but can also robustly capture shock waves in the discontinuous regions. Jiang and Shu² proposed a classical smoothness indicator to calculate the nonlinear weights, with which the WENO (WENO-JS) scheme constructed from the r th order essentially nonoscillatory (ENO) scheme can obtain $(2r - 1)$ th order accuracy. A class of WENO schemes higher than the fifth order is designed by Balsara and Shu³ and by Gerolymos et al.⁴

Henrick et al⁵ derived the necessary and sufficient conditions (NSC) for fifth-order convergence of a fifth-order WENO scheme and pointed out that the fifth-order WENO-JS scheme was reduced to the third-order accuracy at critical points where the first derivative vanishes, and then, the WENO-M scheme was constructed by modifying the weights of WENO-JS with a mapping function. Borges et al⁶ proposed the WENO-Z scheme by constructing a high-order smoothness indicator to compute the nonlinear weights. Castro et al⁷ constructed higher order WENO-Z schemes. Ha et al⁸ and Fan et al⁹ further improved the accuracy of WENO-Z by constructing higher order global smoothness indicators and developed the WENO-NS and WENO-Z η schemes, respectively. On the other hand, Levy et al¹⁰⁻¹² presented a series of central WENO schemes, in which a two-dimensional (2D) high-order interpolant is reconstructed from cell averages by taking a

convex combination of building blocks. Martin et al¹³ proposed a symmetric WENO method by means of a new candidate stencil. Balsara et al¹⁴ developed a new class of WENO schemes with adaptive order for hyperbolic conservation laws.

Different from improving the accuracy of fifth-order WENO schemes at critical points, Shen and Zha¹⁵ first pointed out that the accuracy of the traditional fifth-order WENO schemes is of only second order at transition point (connecting a smooth region and a discontinuity point) and then introduced two fourth-order fluxes combined with an estimation of smoothness/nonsmoothness of two adjacent four-point stencils to improve the accuracy near discontinuities. Subsequently, Shen et al¹⁶ developed a multistep WENO scheme, which can improve the accuracy of the fifth-order WENO schemes near discontinuities without reducing the accuracy in smooth regions even at critical points. Peng and Shen¹⁷ extended the multistep strategy to improve the accuracy of the compact reconstructed WENO (CRWENO) scheme¹⁸ at transition points. However, in the multistep WENO scheme, six weights are calculated and the mapping function proposed by Henrick et al⁵ is needed, which make the algorithm inefficient. In order to enhance the computational efficiency of the multistep WENO scheme, Ma et al¹⁹ proposed an improved multistep WENO scheme and its extension to higher orders of accuracy. Compared with the multistep WENO scheme, although the improved scheme can greatly improve the computational efficiency, the numerical results show that it cannot effectively reduce the dissipation near the discontinuities and its accuracy at critical point is of fourth order. Recently, van Lith et al²⁰ developed a class of embedded WENO scheme. The scheme is simple and provides a choice to improve the accuracy of the WENO-Z scheme at a transition point. In fact, the corresponding embedded WENO-Z scheme is equivalent to multiplying local smoothness indicators by different constants. However, this way, may make the unbalanced contribution of the three substencils of fifth-order WENO scheme and hence results in accuracy decreased in smooth regions. How to develop high performance multistep WENO schemes is still an open issue.

In this paper, based on the analysis of the existing WENO schemes, we further develop the multistep weighting method. Analysis shows that the new method improves the accuracy at transition points, and the calculated weights satisfy the NSCs for the fifth-order convergence in smooth regions even at critical points. Meanwhile, similar to the improved multistep WENO scheme proposed by Ma et al,¹⁹ the present method only needs to calculate three nonlinear weights and does not require a mapping function, which makes the algorithm more efficient than the original multistep WENO scheme.

The rest of this paper is organized as follows: several conventional fifth-order WENO schemes and accuracy analysis of transition point are briefly introduced in Section 2. The new scheme is proposed and a detailed analysis about its accuracy at both critical and transition points is given in Section 3. In Section 4, several numerical examples are presented to demonstrate the efficiency, robustness, and low dissipation properties of the proposed scheme. Some conclusions of this paper are given in Section 5.

2 | FIFTH-ORDER WENO SCHEMES

In this section, the one-dimensional hyperbolic conservation laws is used as a model equation to describe the numerical method

$$\frac{\partial u}{\partial t} + \frac{\partial f(u)}{\partial x} = 0, \quad (1)$$

where $u(x, t)$ is the conservative variable, and $f(u)$ is the flux function.

The semidiscretization form of Equation (1) can be written as

$$\frac{du_i}{dt} = -\frac{\hat{f}_{i+1/2} - \hat{f}_{i-1/2}}{\Delta x}, \quad (2)$$

where Δx is an uniform grid size, $\hat{f}_{i\pm 1/2}$ is the numerical flux.

2.1 | The traditional fifth-order WENO schemes

The numerical flux of a fifth-order WENO scheme can be written as

$$\hat{f}_{i+\frac{1}{2}} = \sum_{k=0}^2 \omega_k \hat{f}_{i+\frac{1}{2}}^k, \quad (3)$$

where $\hat{f}_{i+1/2}^k$ is the third-order flux on the substencil $S_k = \{i+k-2, i+k-1, i+k\}$, and given by

$$\begin{cases} \hat{f}_{i+1/2}^0 = \frac{1}{3}f_{i-2} - \frac{7}{6}f_{i-1} + \frac{11}{6}f_i, \\ \hat{f}_{i+1/2}^1 = -\frac{1}{6}f_{i-1} + \frac{5}{6}f_i + \frac{1}{3}f_{i+1}, \\ \hat{f}_{i+1/2}^2 = \frac{1}{3}f_i + \frac{5}{6}f_{i+1} - \frac{1}{6}f_{i+2}, \end{cases} \quad (4)$$

ω_k is the nonlinear weights. In the work of Jiang and Shu,² the weight function is defined as

$$\omega_k = \frac{\alpha_k}{\alpha_0 + \alpha_1 + \alpha_2}, \quad \alpha_k = \frac{c_k}{(\beta_k + \varepsilon)^2}, \quad k = 0, 1, 2, \quad (5)$$

where $c_0 = \frac{1}{10}$, $c_1 = \frac{6}{10}$, $c_2 = \frac{3}{10}$ are the ideal weights. The parameter ε is introduced to avoid the division by zero. A detailed analysis in the work of Henrick et al⁵ shows that the relatively large value for parameter ε has an influence on the accuracy of the WENO scheme, especially near critical points. Henrick et al⁵ suggested a value of ε slightly larger than the square root of the smallest positive number allowed for a particular machine. Even so, in order to achieve better order of accuracy, in the more recent literatures,²¹⁻²³ there have been a lot of improvements on the choice of ε , for example, the parameter ε is taken as a function of Δx . β_k is the smoothness indicator on substencil S_k . Jiang and Shu² proposed a classical formula for β_k as follows:

$$\beta_k = \sum_{l=1}^{r-1} \int_{x_{i-\frac{1}{2}}}^{x_{i+\frac{1}{2}}} (\Delta x)^{2l-1} \left(\frac{d^l \hat{f}^k(x)}{dx^l} \right)^2 dx. \quad (6)$$

The explicit form of β_k for the fifth-order WENO scheme ($r = 3$) can be expressed as

$$\begin{aligned} \beta_0 &= \frac{13}{12}(f_{i-2} - 2f_{i-1} + f_i)^2 + \frac{1}{4}(f_{i-2} - 4f_{i-1} + 3f_i)^2, \\ \beta_1 &= \frac{13}{12}(f_{i-1} - 2f_i + f_{i+1})^2 + \frac{1}{4}(f_{i+1} - f_{i-1})^2, \\ \beta_2 &= \frac{13}{12}(f_i - 2f_{i+1} + f_{i+2})^2 + \frac{1}{4}(3f_i - 4f_{i+1} + f_{i+2})^2, \end{aligned} \quad (7)$$

and their Taylor series expansions at x_i are

$$\begin{aligned} \beta_0 &= f_i'^2 \Delta x^2 + \left(\frac{13}{12} f_i''^2 - \frac{2}{3} f_i' f_i''' \right) \Delta x^4 + \left(-\frac{13}{6} f_i'' f_i''' + \frac{1}{2} f_i' f_i^{(4)} \right) \Delta x^5 + O(\Delta x^6), \\ \beta_1 &= f_i'^2 \Delta x^2 + \left(\frac{13}{12} f_i''^2 + \frac{1}{3} f_i' f_i''' \right) \Delta x^4 + O(\Delta x^6), \\ \beta_2 &= f_i'^2 \Delta x^2 + \left(\frac{13}{12} f_i''^2 - \frac{2}{3} f_i' f_i''' \right) \Delta x^4 + \left(\frac{13}{6} f_i'' f_i''' - \frac{1}{2} f_i' f_i^{(4)} \right) \Delta x^5 + O(\Delta x^6). \end{aligned} \quad (8)$$

Henrick et al⁵ provided a detailed analysis about the accuracy of the fifth-order WENO scheme of Jiang and Shu (WENO-JS) and derived the NSCs on the weights for fifth-order convergence as

$$\sum_{k=0}^2 A_k (\omega_k^+ - \omega_k^-) = O(\Delta x^3), \quad (9a)$$

$$\omega_k^\pm - c_k = O(\Delta x^2), \quad (9b)$$

and a simple sufficient condition, which is given as

$$\omega_k^\pm - c_k = O(\Delta x^3), \quad (10)$$

where the superscripts \pm correspond to the numerical fluxes $\hat{f}_{i\pm 1/2}$, respectively. In order to satisfy the aforementioned conditions, a mapping function is proposed in the work of Henrick et al⁵ as

$$g_k(\omega) = \frac{\omega (c_k + c_k^2 - 3c_k \omega + \omega^2)}{c_k^2 + \omega(1 - 2c_k)}, \quad (11)$$

and an improved WENO (WENO-M) scheme is developed by using $g_k(\omega)$.

Borges et al⁶ proposed a simple way to calculate the weights as

$$\omega_k = \frac{\alpha_k}{\alpha_0 + \alpha_1 + \alpha_2}, \quad \alpha_k = c_k \left(1 + \left(\frac{\tau_5}{\beta_k + \varepsilon} \right)^q \right), \quad k = 0, 1, 2, \quad (12)$$

where $\tau_5 = |\beta_0 - \beta_2|$ can be called as a high-order smoothness indicator. In smooth regions, the Taylor expansion of τ_5 at x_i gives

$$\tau_5 = \begin{cases} \left| \frac{13}{3} f_i'' f_i''' - f_i' f_i^{(4)} \right| \Delta x^5 + O(\Delta x^7), & f_i' \neq 0, \\ \left| \frac{13}{3} f_i'' f_i''' \right| \Delta x^5 + O(\Delta x^7), & f_i' = 0. \end{cases} \quad (13)$$

As analyzed by Borges et al,⁶ the convergence order of this new WENO (WENO-Z) scheme at critical points is fourth and fifth orders if the power q takes the value of 1 and 2, respectively. However, for solutions containing the discontinuities, increasing q makes the scheme more dissipative.

2.2 | Accuracy analysis at transition point

Shen and Zha¹⁵ provided a detailed analysis about the accuracy of fifth-order WENO schemes near discontinuities and found that they fail to get the optimal order at transition points (see Figure 1).

For completeness, we briefly analyze the accuracy of the transition point here. Without loss of generality, we assume that a discontinuity is located at $[x_{i+1}, x_{i+2}]$ (see Figure 1), ie, the rightmost stencil $S_2 = \{x_i, x_{i+1}, x_{i+2}\}$ of the fifth-order WENO scheme. In this situation, analysis in the work of Shen and Zha¹⁵ shows that the nonlinear weight ω_2 of the WENO-JS or WENO-Z scheme decreases to an essentially zero value, whereas ω_0 and ω_1 approach $\frac{1}{7}$ and $\frac{6}{7}$, respectively. Therefore, applying Taylor series expansion, Equation (3) can be written as

$$\hat{f}_{i+\frac{1}{2}} = \frac{1}{7} \hat{f}_{i+\frac{1}{2}}^0 + \frac{6}{7} \hat{f}_{i+\frac{1}{2}}^1 = \frac{2f_{i-2} - 13f_{i-1} + 41f_i + 12f_{i+1}}{42} = h_{i+\frac{1}{2}} + O(\Delta x^3). \quad (14)$$

However, for calculating the flux $\hat{f}_{i-\frac{1}{2}}$, the stencil $S_5 = \{x_{i-3}, x_{i-2}, \dots, x_{i+1}\}$ is smooth; hence, the fifth-order numerical flux can be obtained as

$$\hat{f}_{i-\frac{1}{2}} = \frac{2f_{i-3} - 13f_{i-2} + 47f_{i-1} + 27f_i - 3f_{i+1}}{60} = h_{i-\frac{1}{2}} + O(\Delta x^5). \quad (15)$$

Subtracting Equation (14) from Equation (15) gives

$$\frac{\hat{f}_{i+\frac{1}{2}} - \hat{f}_{i-\frac{1}{2}}}{\Delta x} = f_i' + O(\Delta x^2). \quad (16)$$

From Equation (16), we can see that the accuracy of the WENO-JS and WENO-Z schemes at transition point is of only second order. As pointed out in the work of Shen et al,¹⁶ a fourth-order numerical flux can be constructed by using a

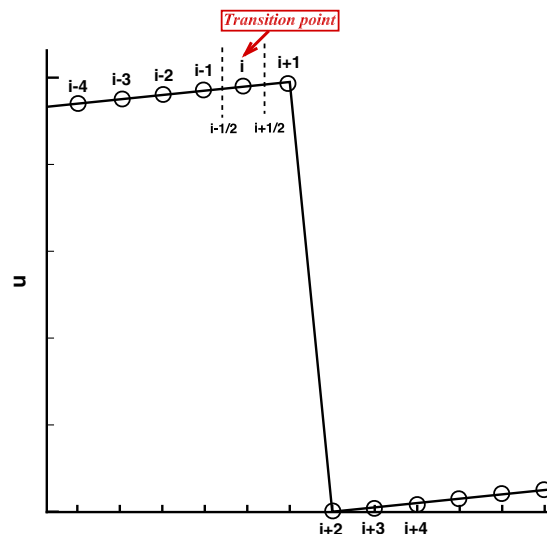


FIGURE 1 The sketch of transition point [Colour figure can be viewed at wileyonlinelibrary.com]

smooth stencil with four points. That is to say, in the smooth stencil $S_4 = \{x_{i-2}, x_{i-1}, x_i, x_{i+1}\}$, the numerical flux $\hat{f}_{i+\frac{1}{2}}$ can be rewritten as

$$\hat{f}_{i+\frac{1}{2}} = c_0^{4,0} \hat{f}_{i+\frac{1}{2}}^0 + c_1^{4,0} \hat{f}_{i+\frac{1}{2}}^1 = \frac{f_{i-2} - 5f_{i-1} + 13f_i + 3f_{i+1}}{12} = h_{i+\frac{1}{2}} + O(\Delta x^4), \quad (17)$$

where $c_0^{4,0} = \frac{1}{4}$, $c_1^{4,0} = \frac{3}{4}$ are the optimal weights.

Hence, subtracting Equation (17) from Equation (15) yields

$$\frac{\hat{f}_{i+\frac{1}{2}} - \hat{f}_{i-\frac{1}{2}}}{\Delta x} = f'_i + O(\Delta x^3). \quad (18)$$

Comparing Equation (16) with Equation (18), we can see that the accuracy at transition point is improved by one order. A symmetric scenario, which the discontinuity is present at $[x_{i-2}, x_{i-1}]$, ie, the leftmost stencil $S_0 = \{x_{i-2}, x_{i-1}, x_i\}$ of the fifth-order WENO scheme, can be analyzed similarly as above.

2.3 | Improvements of the accuracy at transition point

2.3.1 | Hybrid method

In the work of Shen and Zha,¹⁵ a new method is proposed to improve the accuracy at transition point and given as

$$\hat{f}_{i+\frac{1}{2}} = \begin{cases} \bar{h}_0, & \text{if } \tau_4^0 \leq \min(\beta_0, \beta_1, \beta_2) \text{ and } \tau_4^1 > \min(\beta_0, \beta_1, \beta_2), \\ \bar{h}_1, & \text{if } \tau_4^0 > \min(\beta_0, \beta_1, \beta_2) \text{ and } \tau_4^1 \leq \min(\beta_0, \beta_1, \beta_2), \\ h^{\text{WENO-Z}}, & \text{otherwise,} \end{cases} \quad (19)$$

where

$$\begin{cases} \bar{h}_0 = \frac{1}{12} (f_{i-2} - 5f_{i-1} + 13f_i + 3f_{i+1}), \\ \bar{h}_1 = \frac{1}{12} (-f_{i-1} + 7f_i + 7f_{i+1} - 3f_{i+2}) \end{cases} \quad (20)$$

are two fourth-order fluxes. τ_4^0 and τ_4^1 are defined as $\tau_4^0 = |\beta_0 - \beta_1|$ and $\tau_4^1 = |\beta_1 - \beta_2|$, respectively. $h^{\text{WENO-Z}}$ denotes the flux of the WENO-Z scheme. Numerical results in the works of Shen and Zha¹⁵ demonstrate that the new method is more accurate to resolve the flow solutions near discontinuities.

2.3.2 | Multistep WENO scheme

In order to remove the logical statements and construct a better performance scheme, Shen et al¹⁶ developed a multistep WENO scheme which synthetically improved the accuracy of the traditional fifth-order WENO schemes at both critical and transition points. In the first step, two fourth-order fluxes are constructed as

$$\begin{cases} h_0^4 = \omega_0^{4,0} \hat{f}_{i+\frac{1}{2}}^0 + \omega_1^{4,0} \hat{f}_{i+\frac{1}{2}}^1, \\ h_1^4 = \omega_0^{4,1} \hat{f}_{i+\frac{1}{2}}^1 + \omega_1^{4,1} \hat{f}_{i+\frac{1}{2}}^2, \end{cases} \quad (21)$$

where

$$\omega_k^{4,l} = \frac{g_k(\psi_k^{4,l})}{\sum_k g_k(\psi_k^{4,l})}, \quad \psi_k^{4,l} = \frac{\alpha_k^{4,l}}{\sum_k \alpha_k^{4,l}}, \quad \alpha_k^{4,l} = c_k^{4,l} \left(1 + \frac{|\beta_{l+1} - \beta_l|}{\beta_{l+k} + \varepsilon} \right), \quad k, l = 0, 1. \quad (22)$$

$c_0^{4,0}$ and $c_1^{4,0}$ are defined in Equation (17); $c_0^{4,1} = \frac{1}{2}$, $c_1^{4,1} = \frac{1}{2}$ are the optimal weights; $g_k(x)$ is a mapping function in Equation (11). In the second step, the final fifth-order flux is obtained as

$$\hat{f}_{i+\frac{1}{2}} = \omega_0 h_0^4 + \omega_1 h_1^4, \quad (23)$$

where

$$\omega_k = \frac{g_k(\psi_k)}{\sum_k g_k(\psi_k)}, \quad \psi_k = \frac{\alpha_k}{\sum_k \alpha_k}, \quad \alpha_k = d_k \left(1 + \frac{\tau_5}{\beta_k + \varepsilon} \right), \quad k = 0, 1. \quad (24)$$

$d_0 = \frac{2}{5}$, $d_1 = \frac{3}{5}$ are the optimal weights; τ_5 is the global smoothness indicator of the WENO-Z scheme.

Referring to the work of Shen et al,¹⁶ it is easy to see that

$$\omega_k^{4,l} = \begin{cases} c_k^{4,l} + O(\Delta x^6), & f'_i \neq 0, \\ c_k^{4,l} + O(\Delta x^3), & f'_i = 0, \end{cases} \quad (25)$$

and

$$\omega_k = \begin{cases} d_k + O(\Delta x^9), & f'_i \neq 0, \\ d_k + O(\Delta x^3), & f'_i = 0. \end{cases} \quad (26)$$

Equation (25) shows that the flux of the multistep WENO scheme can approximate the flux \bar{h}_0^{-4} and \bar{h}_1^{-4} in Equation (20) if a discontinuity is located at $[x_{i+1}, x_{i+2}]$ and $[x_{i-2}, x_{i-1}]$, respectively. Meanwhile, from Equation (26), we can see that the weights of the multistep WENO scheme satisfy the sufficient condition for the fifth-order convergence in smooth regions even at critical points.

2.3.3 | Embedded WENO-Z scheme

Recently, van Lith et al²⁰ proposed a new method to improve the WENO-Z scheme. Their formula for calculating the weights is

$$\omega_k = \frac{\alpha_k^E}{\alpha_0^E + \alpha_1^E + \alpha_2^E}, \quad \alpha_k^E = c_k \left(1 + \mu \tilde{c}_k \left(\frac{\tau_5}{\beta_k + \varepsilon} \right)^q \right), \quad k = 0, 1, 2, \quad (27)$$

where parameters c_k , β_k , τ_5 , and ε are the same to the ones of the WENO-Z scheme in Equation (12), $\mu = \frac{1}{4}$, $q = 2$; $\tilde{c}_1 = 1$, $\tilde{c}_0 = \tilde{c}_2 = 2$ is based on the consideration of improving the accuracy at transition point. Equation (27) shows that the embedded WENO-Z (E-WENO) scheme is equivalent to multiplying local smoothness indicators by different constants, ie, $\beta'_k = \mu_k \beta_k$ ($\mu_0 = \mu_2 = \frac{\sqrt{2}}{2}$, $\mu_1 = \frac{1}{2}$).

2.3.4 | Improved multistep WENO scheme

In order to reduce the computational cost of the multistep WENO scheme, Ma et al¹⁹ proposed an improved fifth-order multistep WENO (IM-WENO) scheme, in which, the unnormalized weights are defined as

$$\begin{cases} \alpha_0 = c_0 \left(1 + \frac{\tau_5}{\beta_0 + \varepsilon} \right), \\ \alpha_1 = c_1 \left(1 + \frac{\tau_5}{\beta_0 + \beta_1 + \varepsilon} + \frac{\tau_5}{\beta_1 + \beta_2 + \varepsilon} \right), \\ \alpha_2 = c_2 \left(1 + \frac{\tau_5}{\beta_2 + \varepsilon} \right), \end{cases} \quad (28)$$

where parameters c_k , β_k , τ_5 , and ε are the same as the ones of the WENO-Z scheme in Equation (12)).

3 | THE NEW WENO SCHEME

3.1 | The accuracy of E-WENO and IM-WENO

For a smooth solution, by using the Taylor series expansion of β_k (8) and τ_5 (13), the unnormalized weights of the WENO-Z scheme in Equation (12) can be written as

$$\alpha_k = c_k (1 + B \Delta x^r + O(\Delta x^{r+1})), \quad (29)$$

where B is independent of k , and $r = 3q$ and q for $f'_i \neq 0$ and $f'_i = 0$, respectively.

Hence, for the WENO-Z scheme, there is

$$\begin{aligned}\omega_k &= \frac{c_k (1 + B\Delta x^r + O(\Delta x^{r+1}))}{c_0(1 + B\Delta x^r + O(\Delta x^{r+1})) + c_1 (1 + B\Delta x^r + O(\Delta x^{r+1})) + c_2 (1 + B\Delta x^r + O(\Delta x^{r+1}))} \\ &= c_k + O(\Delta x^{r+1}).\end{aligned}\quad (30)$$

After a simple derivation, it can be found that the Taylor series expansion of the unnormalized weights Equation (28) of the IM-WENO scheme is the same as Equation (29) with $q = 1$. Hence, the IM-WENO scheme has the same order as the WENO-Z scheme with $q = 1$.

For the E-WENO scheme, the unnormalized weights α_k^E give

$$\alpha_k^E = c_k (1 + B_k \Delta x^r + O(\Delta x^{r+1})), \quad (31)$$

with the parameters μ_k given in the work of van Lith et al,²⁰ there is

$$B_0 = B_2 \neq B_1; \quad (32)$$

hence, we have

$$\omega_k = c_k + O(\Delta x^r). \quad (33)$$

That means, compared with WENO-Z and IM-WENO, the E-WENO scheme decreases one order for the weights approximating to the ideal weights.

For a solution that contains a discontinuity, for example, which is located at $[x_{i+1}, x_{i+2}]$, we can analyze the properties of E-WENO and IM-WENO at transition point x_i . The E-WENO scheme is taken as an example and the parameter ε takes 0 (since the value of ε should not destroy the ENO property and in order to simplify the analysis).

Since the discontinuity is located at $[x_{i+1}, x_{i+2}]$, we have

$$\beta_2 = O(1), \quad \beta_k = \begin{cases} f_i'^2 \Delta x^2 + O(\Delta x^4), & f_i' \neq 0, \\ \frac{13}{12} f_i'^2 \Delta x^4 + O(\Delta x^5), & f_i' = 0, \end{cases} \quad k = 0, 1, \text{ and } \tau_5 = O(1), \quad (34)$$

that means

$$\beta_2 \gg \beta_0, \beta_1, \quad (35)$$

and hence, $\omega_2 \rightarrow 0$.

Next, we analyze the weights ω_0 . By using Equation (27), ω_0 is calculated as

$$\omega_0 = \frac{c_0 \left(1 + \mu \tilde{c}_0 \left(\frac{\tau_5}{\beta_0}\right)^q\right)}{1 + \mu c_0 \tilde{c}_0 \left(\frac{\tau_5}{\beta_0}\right)^q + \mu c_1 \left(\frac{\tau_5}{\beta_1}\right)^q + \mu c_2 \tilde{c}_2 \left(\frac{\tau_5}{\beta_2}\right)^q}. \quad (36)$$

Multiplying the numerator and denominator of the right-hand term of Equation (36) by $1/(\mu \tilde{c}_0 (\frac{\tau_5}{\beta_0})^q)$, it can be simplified as

$$\omega_0 = \frac{c_0 \left(1 + \frac{1}{\mu \tilde{c}_0} \left(\frac{\beta_0}{\tau_5}\right)^q\right)}{c_0 + \frac{c_1}{\tilde{c}_0} \left(\frac{\beta_0}{\beta_1}\right)^q + \frac{1}{\mu \tilde{c}_0} \left(\frac{\beta_0}{\tau_5}\right)^q + \frac{c_2 \tilde{c}_2}{\tilde{c}_0} \left(\frac{\beta_0}{\beta_2}\right)^q}. \quad (37)$$

Substituting Equation (34) and $\tilde{c}_0 = 2$ into Equation (37), we obtain

$$\omega_0 = \frac{c_0 + O(\Delta x^{r_1})}{c_0 + \frac{1}{2} c_1 (1 + O(\Delta x^{r_2})) + O(\Delta x^{r_1})}, \quad (38)$$

where, for analyzing convenience, we directly express β_0/β_1 as $1 + O(\Delta x^{r_2})$ in Equation (38).

Since $c_0 = 1/10$, $c_1 = 6/10$, we have

$$\omega_0 = c_0^{4,0} + O(\Delta x^r), \quad (39)$$

where $c_0^{4,0} = 1/4$ and $r = \min(r_1, r_2)$. According to Equation (34), it is easy to find that

$$r_1 = \begin{cases} 2q, & f'_i \neq 0, \\ 4q, & f'_i = 0. \end{cases} \quad (40)$$

Clearly, $q = 2$ can improve the accuracy of the numerator. The key problem is how to improve the accuracy of the denominator. Since $\beta_2 = O(1)$ and $\tau_5 = O(1)$, it is clear that r_2 is decided by β_0/β_1 . From Equation (8), for a smooth solution, there is

$$\frac{\beta_k}{\beta_j} = \begin{cases} 1 + O(\Delta x^2), & f'_i \neq 0, \\ 1 + O(\Delta x), & f'_i = 0, \end{cases} \quad k \neq j. \quad (41)$$

A similar formula holds for the two smooth stencils at transition point. Hence, one has that

$$r_2 = \begin{cases} 2, & f'_i \neq 0, \\ 1, & f'_i = 0. \end{cases} \quad (42)$$

Similarly, we can analyze ω_1 . Hence, we get

$$\omega_k = \begin{cases} c_k^{4,0} + O(\Delta x^2), & f'_i \neq 0, \\ c_k^{4,0} + O(\Delta x), & f'_i = 0, \end{cases} \quad k = 0, 1. \quad (43)$$

The IM-WENO scheme can be analyzed similarly, and the same conclusion Equation (43) can be drawn. Please notice that the formula equation (43) is independent of the power q .

Equation (43) indicates that both the E-WENO and IM-WENO schemes can theoretically approximate the fourth-order flux \overleftarrow{h}_0 in Equation (20) when the discontinuity is located at $[x_{i+1}, x_{i+2}]$. However, numerical results in the works of Ma et al¹⁹ and van Lith et al²⁰ and in this paper show that the E-WENO and IM-WENO schemes cannot effectively reduce the dissipation of WENO-Z near the discontinuities. This paper will further develop multistep WENO scheme, which can obtain high-order accuracy in smooth regions and can also decrease the dissipation near the discontinuities.

3.2 | The new weighting method

As indicated above, theoretically, the idea of multistep weighting is helpful for improving the accuracy at transition point. However, limited by the condition of $(\beta_k/\beta_j, k \neq j)$, the simple linear combination of different β , such as the formula of Ma et al¹⁹ and van Lith et al,²⁰ cannot achieve the expected effects. Hence, we propose a new method by using a function $h(\beta_l, \beta_1) (l = 0, 2)$ to replace $\beta_l + \beta_1$ in Equation (28), and the function should satisfy

$$h(\beta_l, \beta_1) = \begin{cases} 2\beta_l + O(\Delta x^{\tilde{N}}), & \text{if } S_4^l \text{ is a smooth stencil,} \\ \sim \beta_1, & \beta_l \ll \beta_1, \end{cases} \quad (44)$$

where $S_4^0 = \{x_{i-2}, \dots, x_{i+1}\}$, $S_4^2 = \{x_{i-1}, \dots, x_{i+2}\}$, and larger \tilde{N} gives better accuracy for solutions.

For this purpose, a function $h(\beta_l, \beta_1)$ is suggested as

$$h(\beta_l, \beta_1) = 2\beta_l + \left(\frac{\beta_l - \beta_1}{\beta_l + \beta_1 + \varepsilon} \right)^2 \beta_1, \quad l = 0, 2. \quad (45)$$

Obviously, the new function equation (45) satisfies the requirements in Equation (44), and $\tilde{N} = 6$ for both the cases of $f'_i = 0$ and $f'_i \neq 0$. Then, using Equation (45), a new method for calculating the weights is proposed as

$$\begin{cases} \alpha_0 = c_0 \left(1 + \frac{\tau_5}{\beta_0 + \varepsilon} \right), \\ \alpha_1 = c_1 \left(1 + \frac{\tau_5}{h(\beta_0, \beta_1) + \varepsilon} + \frac{\tau_5}{h(\beta_2, \beta_1) + \varepsilon} \right), \\ \alpha_2 = c_2 \left(1 + \frac{\tau_5}{\beta_2 + \varepsilon} \right), \end{cases} \quad (46)$$

where parameters c_k , β_k , τ_5 , and ε are the same as the ones of the WENO-Z scheme in Equation (12).

Similarly, for the case of the power parameter $q = 2$, the unnormalized weights can be defined as

$$\begin{cases} \alpha_0 = c_0 \left(1 + \frac{\tau_5^2}{\beta_0^2 + \varepsilon} \right), \\ \alpha_1 = c_1 \left(1 + \frac{\tau_5^2}{h(\beta_0^2, \beta_1^2) + \varepsilon} + \frac{\tau_5^2}{h(\beta_2^2, \beta_1^2) + \varepsilon} \right), \\ \alpha_2 = c_2 \left(1 + \frac{\tau_5^2}{\beta_2^2 + \varepsilon} \right). \end{cases} \quad (47)$$

Alternatively, one can even use a simpler form

$$h(\beta_l^2, \beta_1^2) = 2\beta_l^2 + (\beta_l - \beta_1)^2, \quad l = 0, 2. \quad (48)$$

3.3 | Accuracy analysis of the new scheme

Assuming the solution is sufficiently smooth in all candidate stencils, and substituting Equations (8) and (13) into Equation (46), we have

$$\omega_k = \begin{cases} c_k + O(\Delta x^5), & f'_i \neq 0, \\ c_k + O(\Delta x^2), & f'_i = 0. \end{cases} \quad (49)$$

Equation (49) shows that the new weights satisfy the second term of the NSC Equation (9b) for fifth-order convergence in smooth regions even at critical points. Similar to the analysis in the work of Borges et al.,⁶ the first term in the NSC Equation (9a) can be written as

$$\sum_{k=0}^2 A_k (\omega_k^+ - \omega_k^-) = \frac{N^+ D^- - N^- D^+}{D^+ D^-} = O(\Delta x^5), \quad (50)$$

where

$$N^\pm = \tau_5^\pm \prod_{k=0}^2 \bar{\beta}_k^\pm \sum_{k=0}^2 \frac{A_k^\pm c_k}{\bar{\beta}_k^\pm}, \quad D^\pm = \prod_{k=0}^2 \bar{\beta}_k^\pm + \tau_5^\pm \prod_{k=0}^2 \bar{\beta}_k^\pm \sum_{k=0}^2 \frac{c_k}{\bar{\beta}_k^\pm}. \quad (51)$$

$\bar{\beta}_k$ denotes the modified smoothness indicators of the IM-WENO and present schemes. In the IM-WENO scheme,

$$\bar{\beta}_0 = \beta_0, \quad \bar{\beta}_1 = \frac{(\beta_0 + \beta_1)(\beta_1 + \beta_2)}{(\beta_0 + \beta_1) + (\beta_1 + \beta_2)}, \quad \bar{\beta}_2 = \beta_2. \quad (52)$$

In the present scheme,

$$\bar{\beta}_0 = \beta_0, \quad \bar{\beta}_1 = \frac{h(\beta_0, \beta_1)h(\beta_2, \beta_1)}{h(\beta_0, \beta_1) + h(\beta_2, \beta_1)}, \quad \bar{\beta}_2 = \beta_2, \quad (53)$$

where the function h is defined in Equation (45).

Thus, with the aid of a symbolic algebra program by substituting the Taylor series expansion of the smoothness indicators β_k Equation (8), Table 1 gives the value of s in Equation (50). In addition, the process for calculating these values is given in the Appendix.

From Table 1, the first term of the NSC of the IM-WENO scheme is given by

$$\sum_{k=0}^2 A_k (\omega_k^+ - \omega_k^-) = \begin{cases} O(\Delta x^6), & f'_i \neq 0, \\ O(\Delta x^2), & f'_i = 0. \end{cases} \quad (54)$$

TABLE 1 The value of s in Equation (50)

	IM-WENO ¹⁹		Present	
	$f'_i \neq 0$	$f'_i = 0$	$f'_i \neq 0$	$f'_i = 0$
$N^+ D^- - N^- D^+$	$O(\Delta x^{18})$	$O(\Delta x^{26})$	$O(\Delta x^{20})$	$O(\Delta x^{27})$
$D^+ D^-$	$O(\Delta x^{12})$	$O(\Delta x^{24})$	$O(\Delta x^{12})$	$O(\Delta x^{24})$
s	6	2	8	3

However, for the present scheme, there is

$$\sum_{k=0}^2 A_k (\omega_k^+ - \omega_k^-) = \begin{cases} O(\Delta x^8), & f'_i \neq 0, \\ O(\Delta x^3), & f'_i = 0. \end{cases} \quad (55)$$

Equations (49) and (55) indicate that the weights of the present scheme satisfy the NSC for fifth-order convergence in smooth regions including critical points where the first derivative vanishes but the high-order derivative does not, while the weights of the IM-WENO scheme do not satisfy the NSC at critical points, as shown in Equations (30) and (54).

It should be pointed out that, in this paper, only the weighting method with a fixed value for ε (for example, $\varepsilon = 10^{-40}$) is applied, so the fifth-order accuracy can be achieved only for the case with the first critical point where $f' = 0$ and $f'' \neq 0$. For the higher order critical point, similar as the WENO-Z scheme,^{6,9} the new scheme has only second order. In order to obtain high-order convergence rate, one feasible way is to set ε proportionally to Δx to some power²² or design higher order global smoothness indicator.⁹

If the solution is discontinuous on the global stencil, without loss of generality, we assume that the discontinuity is located at $[x_{i+1}, x_{i+2}]$. Similar to the analysis in Section 3.1, we can obtain the values of the parameters r_1 and r_2 in Equation (38) as follows:

$$r_1 = \begin{cases} 2, & f'_i \neq 0, \\ 4, & f'_i = 0, \end{cases} \quad r_2 = \begin{cases} 4, & f'_i \neq 0, \\ 2, & f'_i = 0. \end{cases} \quad (56)$$

Compared with Equations (40) and (42), it is found that the value of r_2 is doubled. Finally, we have

$$\omega_k = \begin{cases} c_k^{4,0} + O(\Delta x^2), & f'_i \neq 0, \\ c_k^{4,0} + O(\Delta x^2), & f'_i = 0, \end{cases} \quad k = 0, 1, \omega_2 \rightarrow 0. \quad (57)$$

Similarly, results can be obtained for the case of the discontinuity located at $[x_{i-2}, x_{i-1}]$. Numerical examples show that this improvement can effectively reduce the dissipation near the discontinuities.

In addition, if the discontinuity is located at $[x_{i-1}, x_i]$ and $[x_i, x_{i+1}]$, the weights of the present scheme are approximated by $\omega_0 \rightarrow 0, \omega_1 \rightarrow 0, \omega_2 \rightarrow 1$, and $\omega_0 \rightarrow 1, \omega_1 \rightarrow 0, \omega_2 \rightarrow 0$, respectively. Therefore, the new WENO scheme can keep the ENO property near shock waves.

4 | NUMERICAL EXAMPLES

In this section, several numerical examples are given to compare the following schemes:

- (1) WENO-Z: Weighting method Equation (12) with $q = 1$ and $\varepsilon = 10^{-40}$;
- (2) WENO-Z2: Weighting method Equation (12) with $q = 2$ and $\varepsilon = 10^{-40}$;
- (3) WENO-Zdx3²²: Weighting method Equation (12) with $q = 1$ and $\varepsilon = \Delta x^3$;
- (4) WENO-Z2dx4²²: Weighting method Equation (12) with $q = 2$ and $\varepsilon = \Delta x^4$;
- (5) M-WENO: Multistep WENO scheme Equation (23) with $\varepsilon = 10^{-40}$;
- (6) E-WENO: Embedded WENO-Z scheme Equation (27) with $\varepsilon = 10^{-40}$;
- (7) IM-WENO: Improved multistep WENO scheme Equation (28) with $\varepsilon = 10^{-40}$;
- (8) IM-WENO-2: IM-WENO scheme with $q = 2$ and $\varepsilon = 10^{-40}$;
- (9) HM-WENO: New WENO scheme Equations (45) and (46) with $\varepsilon = 10^{-40}$;
- (10) HM-WENO-2: New WENO scheme Equations (47) and (48) with $\varepsilon = 10^{-40}$.

The fourth-order Runge-Kutta method²⁴ is used to approximate the time derivative, and the CFL number is set to be 0.5 for all examples in this paper.

4.1 | The accuracy at critical point

Referring to the works of Castro et al⁷ and Fan et al,⁹ the function $f(x) = x^2 e^x$, which has a critical point at $x = 0$ where $f'(0) = 0$ and $f''(0) \neq 0$, is also used to measure the accuracy of the new scheme and several WENO schemes mentioned

TABLE 2 Comparison of errors and convergence orders for different schemes at critical point

Δx	WENO-Z		WENO-Zdx3		M-WENO		IM-WENO		HM-WENO	
	Error	order	Error	order	Error	order	Error	order	Error	order
2e-2	0.496e-06	-	0.844e-08	-	0.154e-08	-	0.286e-06	-	0.265e-07	-
1e-2	0.292e-07	4.09	0.192e-09	5.46	0.496e-10	4.95	0.159e-07	4.17	0.968e-09	4.78
5e-3	0.176e-08	4.05	0.411e-11	5.55	0.156e-11	4.99	0.923e-09	4.11	0.326e-10	4.89
2.5e-3	0.108e-09	4.03	0.915e-13	5.49	0.488e-13	5.00	0.552e-10	4.06	0.106e-11	4.94
1.25e-3	0.666e-11	4.02	0.222e-14	5.37	0.152e-14	5.00	0.337e-11	4.03	0.338e-13	4.97
Δx	WENO-Z2		WENO-Z2dx4		E-WENO		IM-WENO-2		HM-WENO-2	
2e-2	0.256e-06	-	0.127e-06	-	0.138e-05	-	0.194e-06	-	0.461e-08	-
1e-2	0.579e-08	5.47	0.323e-08	5.30	0.817e-07	4.08	0.397e-08	5.61	0.613e-10	6.23
5e-3	0.144e-09	5.33	0.888e-10	5.19	0.500e-08	4.03	0.894e-10	5.47	0.157e-11	5.28
2.5e-3	0.392e-11	5.20	0.258e-11	5.10	0.310e-09	4.01	0.224e-11	5.32	0.482e-13	5.03
1.25e-3	0.113e-12	5.11	0.776e-13	5.06	0.193e-10	4.01	0.615e-13	5.19	0.151e-14	4.99

above. Meanwhile, in order to evaluate the influence of the value of ε on the accuracy of WENO scheme at critical point, ε is taken as the power of Δx employed in the work of Don and Borges²² and a fixed constant 10^{-40} recommended by Henrick et al,⁵ respectively. Table 2 gives the comparison of the errors of the first derivative of the function $f(x)$ at $x = 0$ and convergence orders of different schemes. The critical point is set as a grid point x_i and the flux $\hat{f}_{i+1/2}$ is calculated by using the five-point stencil $[x_{i-2}, x_{i-1}, \dots, x_{i+2}]$, where, $x_i = 0, x_{i \pm n} = x_i \pm n \Delta x$. From this table, we can see that WENO-Zdx3 and WENO-Z2dx4,²² M-WENO,¹⁶ and HM-WENO achieve fifth-order accuracy at critical point. Hence, as analyzed in the work of Don and Borges,²² the WENO-Z scheme can obtain the optimal convergence order at critical point if ε takes the power of Δx . The IM-WENO scheme¹⁹ has the same fourth-order accuracy as the WENO-Z scheme ($q = 1, \varepsilon = 10^{-40}$), although its error is less than WENO-Z's. For the case of the power parameter $q = 2$, the E-WENO scheme is only fourth-order accuracy. As analyzed in Section 3.1, the E-WENO scheme decreases the accuracy of the WENO-Z scheme (with $q = 2$).

4.2 | The errors around transition point

In this subsection, the following function

$$f(x) = \begin{cases} A \sin(k\pi x), & -1 \leq x \leq 0, \\ A \sin(k\pi x) + 1, & 0 < x \leq 1 \end{cases} \quad (58)$$

is used to measure the performance of different schemes mentioned above around transition point, where $A = 0.01, k = 6$. For this case, $x_i = 0$ and the next point x_{i+1} are the discontinuity points. Hence, the points x_{i-1} and x_{i+3} are the transition points. Table 3 gives the comparison of errors of first-order derivative of $f(x)$ in Equation (58) for different schemes around the transition points with $N = 80, N = 160$, and $N = 320$, and the transition points are displayed in bold. It can be seen that the errors of the multistep WENO-type schemes (M-WENO, IM-WENO, IM-WENO-2, E-WENO, HM-WENO, HM-WENO-2) are less than those of WENO-Z-type schemes (WENO-Z, WENO-Z2, WENO-Zdx3, WENO-Z2dx4) at transition points.

4.3 | One-dimensional linear advection problems

The governing equation of linear advection problems is given by

$$\begin{cases} \frac{\partial u}{\partial t} + \frac{\partial u}{\partial x} = 0, \\ u(x, 0) = u_0(x). \end{cases} \quad (59)$$

The periodic boundary condition is applied for this kind of problem.

4.3.1 | The first case of advection equation

The initial condition is given by

$$u_0(x) = \begin{cases} \frac{1}{6} (G(x, \beta, z - \delta) + G(x, \beta, z + \delta) + 4G(x, \beta, z)), & -0.8 \leq x \leq -0.6 \\ 1, & -0.4 \leq x \leq -0.2 \\ 1 - |10(x - 0.1)|, & 0 \leq x \leq 0.2 \\ \frac{1}{6} (F(x, \alpha, a - \delta) + F(x, \alpha, a + \delta) + 4F(x, \alpha, a)), & 0.4 \leq x \leq 0.6 \\ 0, & \text{otherwise,} \end{cases} \quad (60)$$

with the computational domain $[-1, 1]$, where $G(x, \beta, z) = e^{-\beta(x-z)^2}$, $F(x, \alpha, a) = \sqrt{\max(1 - \alpha^2(x - a)^2, 0)}$, $a = 0.5$, $z = -0.7$, $\delta = 0.005$, $\alpha = 10$, and $\beta = \log 2 / 36\delta^2$. The solution contains a Gaussian, a square-wave, a triangle, and a semiellipse wave. Figure 2 gives the numerical results of different schemes. From the enlarged part of this figure, we can find that the

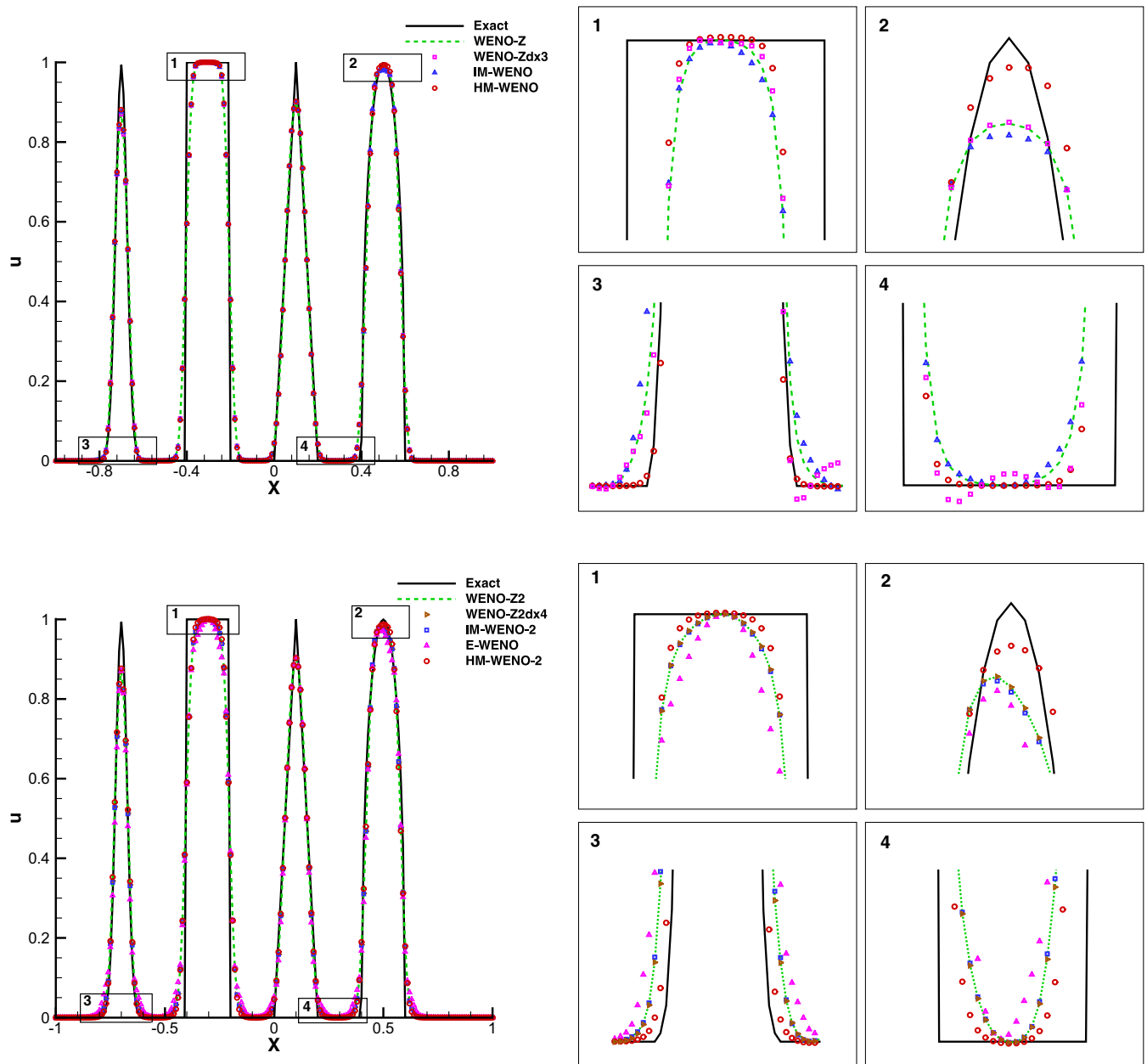


FIGURE 2 Linear advection problem with initial condition Equation (60) at $t = 6$, $N = 200$ [Colour figure can be viewed at wileyonlinelibrary.com]

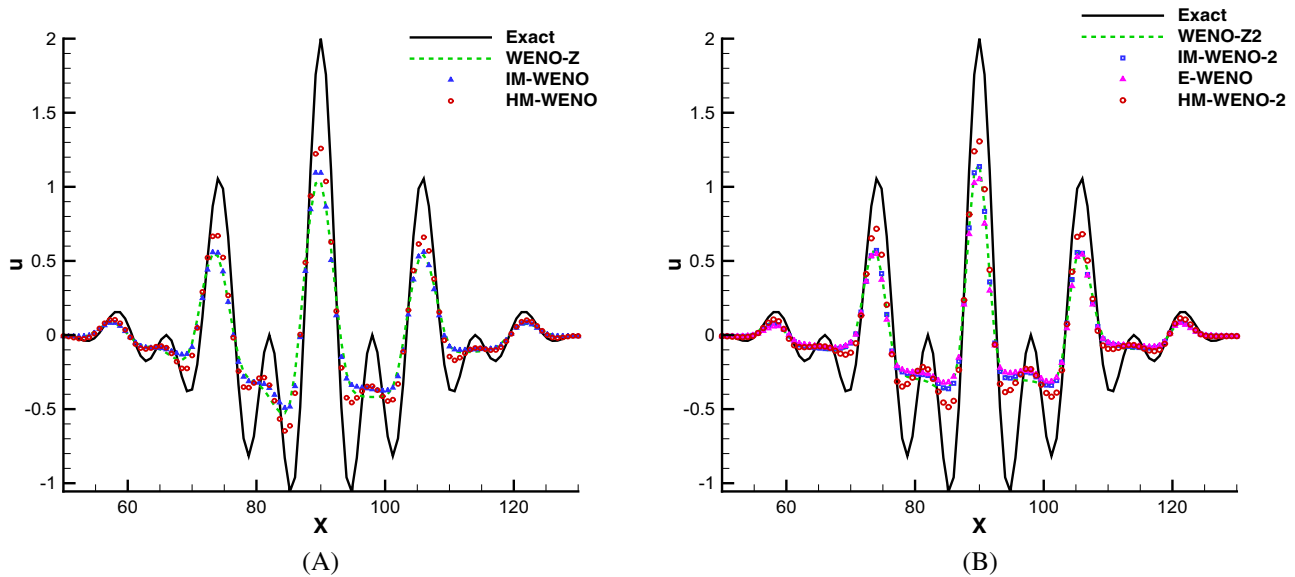


FIGURE 3 Linear advection problem with initial condition Equation (61) with $N = 100$ at (A) $t = 960$, (B) $t = 400$ [Colour figure can be viewed at wileyonlinelibrary.com]

IM-WENO and E-WENO schemes even generate less accurate solution than WENO-Z with $q = 1$ and $q = 2$, respectively. The HM-WENO and HM-WENO-2 schemes can effectively reduce the dissipation near the discontinuities, and they have the best resolution for four kinds of waves.

Apparently, as shown in Section 4.1 and in the work of Don and Borges,²² the WENO-Z (with $\varepsilon = \Omega(\Delta x^m)$) scheme can obtain the optimal convergence order at critical points (even at high-order critical points). However, as stated in the work of Don and Borges,²² for $q = 1$, both the WENO-JS and WENO-Z schemes do not have sufficient numerical dissipation to remove the numerical oscillations from the solution, regardless of the order of schemes and ε chosen. Since this paper mainly focuses on the improvement at transition point, for the rest examples, only the case of $\varepsilon = 10^{-40}$ is discussed and compared, although the improvement strategy is still available for those WENO schemes with $\varepsilon = \Omega(\Delta x^m)$.

4.3.2 | The second case of advection equation

The initial condition is given by

$$u_0(x) = e^{-(x-90)^2/400} \left(\cos\left(\frac{\pi}{8}(x-90)\right) + \cos\left(\frac{\pi}{4}(x-90)\right) \right), \quad 50 \leq x \leq 130. \quad (61)$$

Figure 3 gives the numerical results of different schemes. Similar to the above example, the HM-WENO and HM-WENO-2 schemes apparently improve the accuracy of the solution of the high-frequency wave problem.

Since the comparison and conclusion for those schemes with $q = 2$ are in agreement with those with $q = 1$, in the rest of this paper, only the results of the WENO-Z, IM-WENO, and HM-WENO schemes are shown and discussed.

4.3.3 | The third case of advection equation

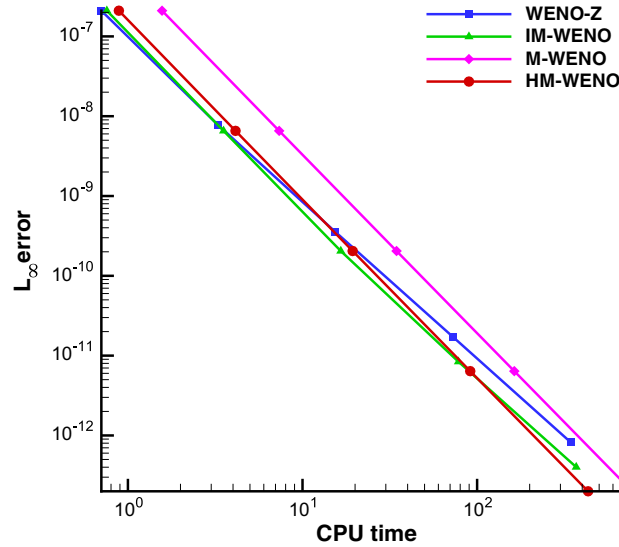
The initial condition is given by⁵

$$u_0(x) = \sin\left(\pi x - \frac{\sin(\pi x)}{\pi}\right), \quad -1 \leq x \leq 1. \quad (62)$$

This solution has two critical points, where $u'(0) = 0$ and $u'''(0) \neq 0$. As in the works of Jiang and Shu² and Ha et al,⁸ the time step is set to $\Delta x^{5/4}$. The program with quadruple precision is performed on Intel Xeon E5-2640 v3. Table 4 gives the errors, convergence orders, and CPU time of different schemes at $t = 2$. From this table, it can be seen that the HM-WENO scheme gets the same fifth-order accuracy as the first multistep WENO (M-WENO) scheme. While the convergence orders of the WENO-Z and IM-WENO schemes gradually decrease to fourth order with refined meshes. The comparisons of computational efficiency are shown in Figure 4. As observed from this figure, the HM-WENO scheme greatly improves the computational efficiency of the M-WENO scheme. It can be seen that HM-WENO costs about 30% and 15% CPU time more than WENO-Z and IM-WENO, respectively; however, if a more accurate solution (with a refined mesh) is required, the HM-WENO scheme is more efficient than both the WENO-Z and IM-WENO schemes.

TABLE 4 Comparison of errors, convergence orders, and CPU time (in seconds) for different schemes

N	WENO-Z		IM-WENO		M-WENO		HM-WENO	
	L_∞ (order)	CPU Time	L_∞ (order)	CPU time	L_∞ (order)	CPU Time	L_∞ (order)	CPU Time
160	0.21e-06(—)	7.0e-01	0.21e-06(—)	7.6e-01	0.21e-06(—)	1.6e+00	0.21e-06(—)	8.9e-01
320	0.78e-08(4.76)	3.3e+00	0.66e-08(5.00)	3.5e+00	0.66e-08(5.00)	7.3e+00	0.66e-08(5.00)	4.1e+00
640	0.36e-09(4.44)	1.5e+01	0.20e-09(5.00)	1.7e+01	0.20e-09(5.00)	3.5e+01	0.20e-09(5.00)	1.9e+01
1280	0.17e-10(4.37)	7.3e+01	0.84e-11(4.61)	7.8e+01	0.64e-11(5.00)	1.6e+02	0.64e-11(5.00)	9.1e+01
2560	0.82e-12(4.39)	3.4e+02	0.40e-12(4.39)	3.7e+02	0.20e-12(5.00)	7.7e+02	0.20e-12(5.00)	4.3e+02

**FIGURE 4** Comparisons of computational efficiency [Colour figure can be viewed at wileyonlinelibrary.com]

4.4 | One-dimensional Euler problems

The governing equation of one-dimensional Euler problems is given by

$$\frac{\partial U}{\partial t} + \frac{\partial F(U)}{\partial x} = 0, \quad (63)$$

where $U = (\rho, \rho u, E)^T$, $F(U) = (\rho u, \rho u^2 + p, u(E + p))^T$; ρ, u, E, p denote the density, velocity, total energy, and pressure, respectively, and for ideal gas $E = \frac{p}{\gamma - 1} + \frac{1}{2} \rho u^2$. $\gamma = 1.4$ is the ratio of specific heat. The global Lax-Friedrichs flux-splitting method with local characteristic reconstruction is used for the inviscid flux.

4.4.1 | Lax problem

The initial conditions of this problem are

$$(\rho, u, p) = \begin{cases} (0.445, 0.698, 3.528), & -5 \leq x < 0 \\ (0.5, 0, 0.571), & 0 \leq x \leq 5, \end{cases} \quad (64)$$

with zero gradient boundary conditions at $x = \pm 5$. Figure 5 gives the numerical results with $N = 200$ at $t = 1.3$. The reference result is obtained by the WENO-Z scheme with refined grids. From the enlarged part of this figure, we can see that the present scheme is more accurate than the other schemes near shock waves.

4.4.2 | Shock entropy wave interaction

The initial conditions of this problem²⁵ are

$$(\rho, u, p) = \begin{cases} (3.857143, 2.629369, 31/3), & -5 \leq x < -4 \\ (1 + 0.2 \sin(5x), 0, 1), & -4 \leq x \leq 5, \end{cases} \quad (65)$$

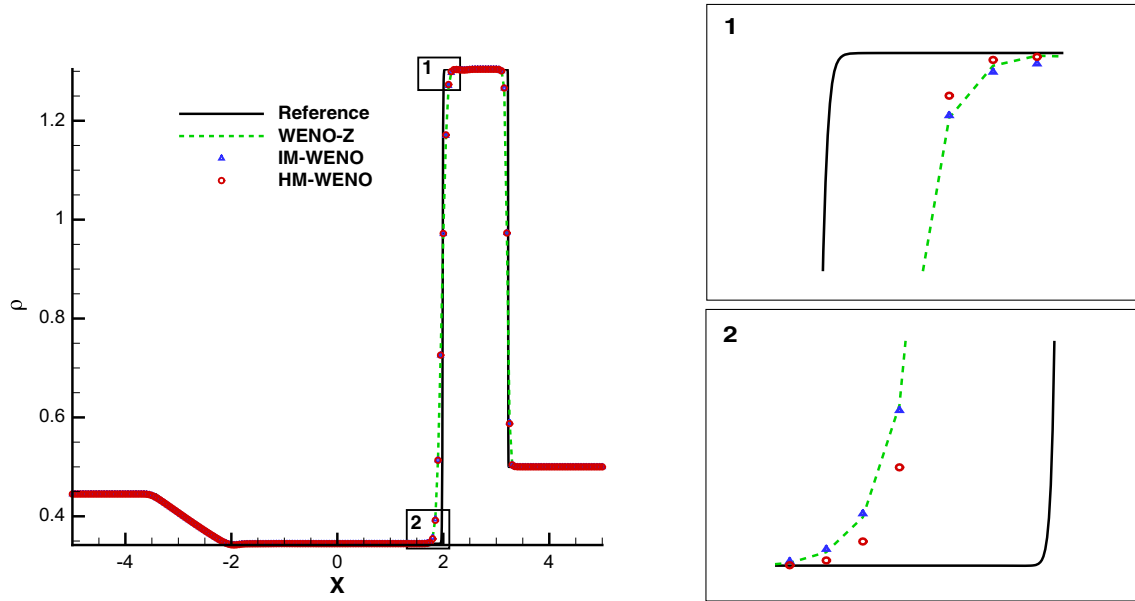


FIGURE 5 Lax problem at $t = 1.3$, $N = 200$ [Colour figure can be viewed at wileyonlinelibrary.com]

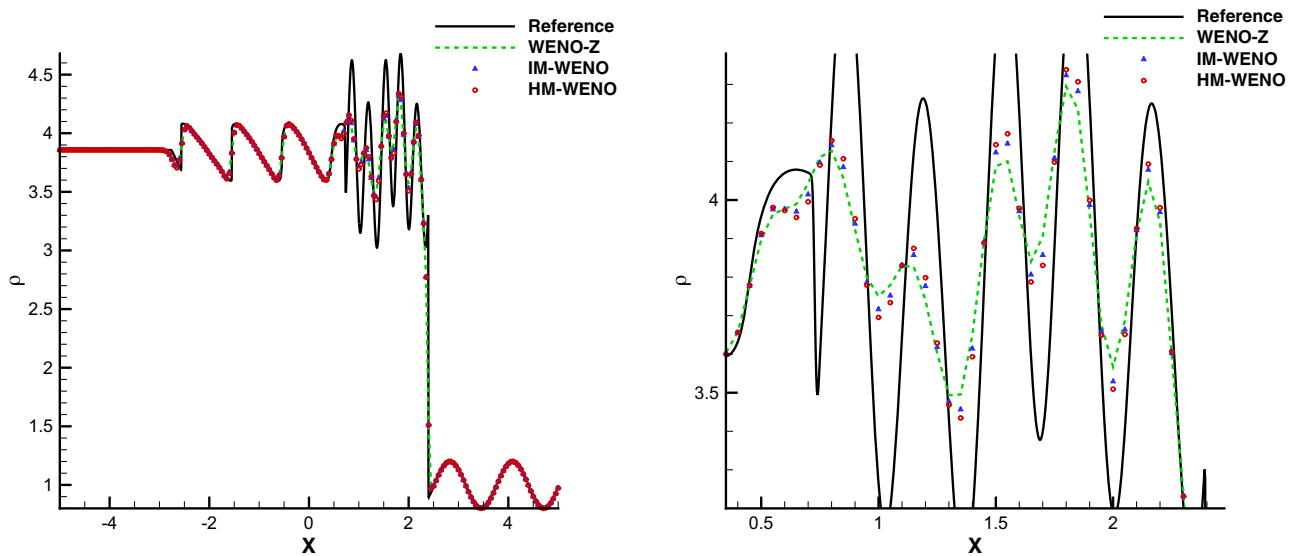


FIGURE 6 Shock entropy wave interaction at $t = 1.8$, $N = 200$ [Colour figure can be viewed at wileyonlinelibrary.com]

with zero gradient boundary conditions at $x = \pm 5$. This case represents a Mach 3 shock wave interacting with a sine entropy wave and is widely used for evaluating the resolution of the shock-capturing schemes. The numerical results of different schemes with $N = 200$ at $t = 1.8$ are shown in Figure 6. This example shows that, for the high frequency waves, the HM-WENO scheme can also obtain more accurate results than the WENO-Z and IM-WENO schemes.

4.4.3 | Interacting blast waves

The initial conditions of this problem^{5,6} are

$$(\rho, u, p) = \begin{cases} (1, 0, 1000), & 0 \leq x < 0.1 \\ (1, 0, 0.01), & 0.1 \leq x < 0.9 \\ (1, 0, 100), & 0.9 \leq x \leq 1, \end{cases} \quad (66)$$

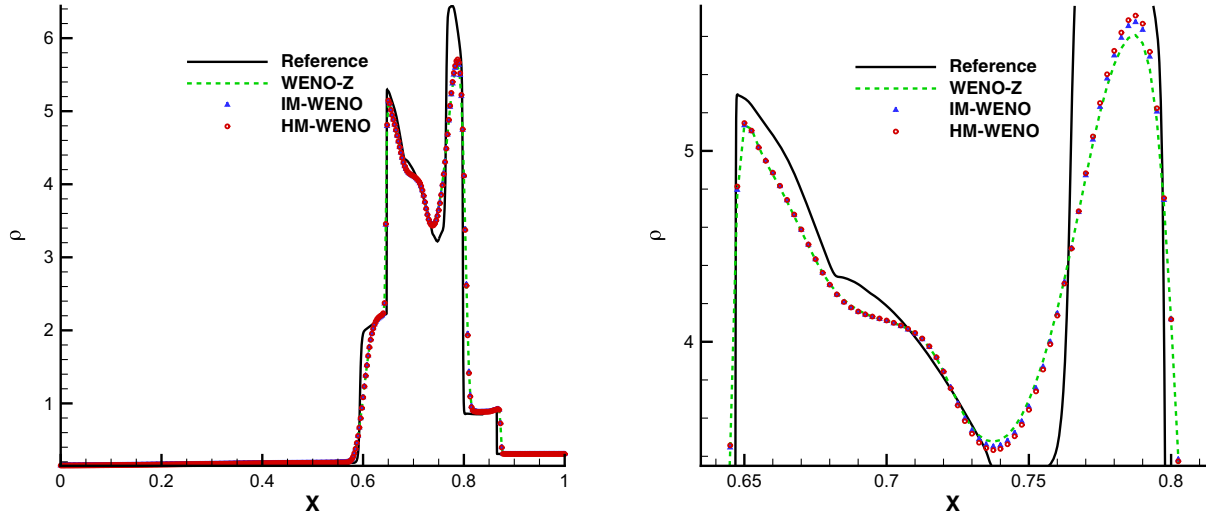


FIGURE 7 Interacting blast waves at $t = 0.038$, $N = 400$ [Colour figure can be viewed at wileyonlinelibrary.com]

with reflection boundary conditions at $x = 0$ and $x = 1$. This case is often used as a benchmark case to test the robustness and the capability of shock-capturing for different schemes. Figure 7 gives the numerical results with $N = 400$ at $t = 0.038$. It can be observed that the present scheme can capture the strong shock as well as the WENO-Z and IM-WENO schemes.

4.5 | 2D Euler problems

The governing equation of 2D Euler problems is given by

$$\frac{\partial U}{\partial t} + \frac{\partial F}{\partial x} + \frac{\partial G}{\partial y} = 0, \quad (67)$$

where

$$U = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ E \end{bmatrix}, \quad F = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho uv \\ Eu + pu \end{bmatrix}, \quad G = \begin{bmatrix} \rho v \\ \rho uv \\ \rho v^2 + p \\ Ev + pv \end{bmatrix}. \quad (68)$$

The specific total energy E is given by

$$E = \frac{p}{(\gamma - 1)} + \frac{1}{2}\rho(u^2 + v^2). \quad (69)$$

The Steger-Warming flux splitting method²⁶ is used for the inviscid convective fluxes. The WENO reconstruction is carried out for each component of the split fluxes. The time step is taken as²⁷

$$\Delta t = CFL \frac{\Delta t_x \Delta t_y}{\Delta t_x + \Delta t_y}, \quad \text{with } \Delta t_x = \frac{\Delta x}{\max_{i,j} (|u_{i,j}| + c_{i,j})} \quad \text{and} \quad \Delta t_y = \frac{\Delta y}{\max_{i,j} (|v_{i,j}| + c_{i,j})}, \quad (70)$$

where c is the speed of sound.

4.5.1 | 2D vortex evolution problem

The 2D vortex evolution problem²⁸ is often used to evaluate the dissipation property of a scheme. It describes an isentropic vortex moves across the computational domain periodically. The initial conditions of this problem are

$$\begin{cases} u = 0.5 - \frac{\varepsilon e^{(1-r^2)/2}}{2\pi} (y - 5), \\ v = \frac{\varepsilon e^{(1-r^2)/2}}{2\pi} (x - 5), \\ T = 1 - \frac{(\gamma-1)\varepsilon^2 e^{(1-r^2)}}{8\gamma\pi^2}, \\ S = 1. \end{cases} \quad (71)$$

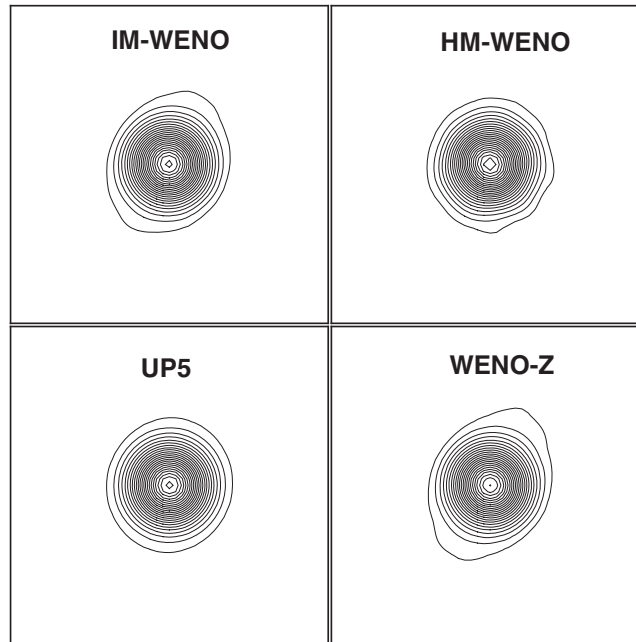


FIGURE 8 Pressure contours of the vortex evolution problem, 30 contours from 0.9918 to 0.9998

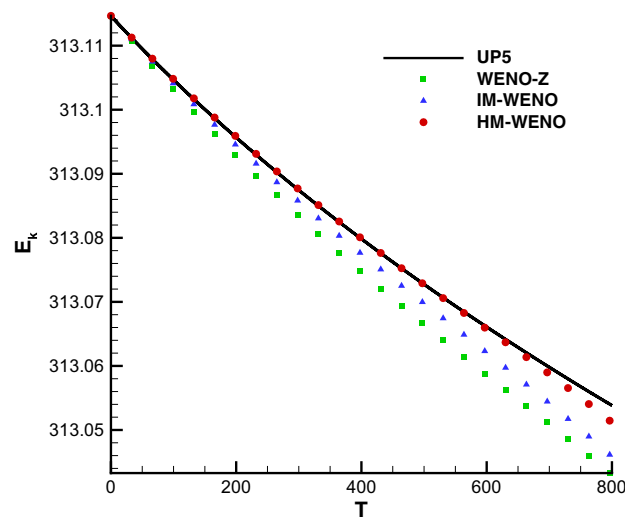


FIGURE 9 Integrated kinetic energy versus time [Colour figure can be viewed at wileyonlinelibrary.com]

The temperature T and entropy S are defined as follows:

$$T = \frac{P}{\rho}, \quad S = \frac{P}{\rho^\gamma},$$

where $r^2 = (x-5)^2 + (y-5)^2$, and vortex strength ε is 0.5. The computational domain is $[0, 10] \times [0, 10]$. Periodic boundary conditions are set for all boundaries. Figure 8 gives the pressure contours of different schemes with $N_x \times N_y = 50 \times 50$ at $t = 800$. The evolution of the integrated kinetic energy ($E_k = \sum_{i,j} \rho_{i,j} (u_{i,j}^2 + v_{i,j}^2) / 2$) is shown in Figure 9. It can be seen that the HM-WENO scheme maintains the symmetry of the vortex structure better than the WENO-Z and IM-WENO schemes, and its results are close to those of the fifth-order upstream scheme (UP5).

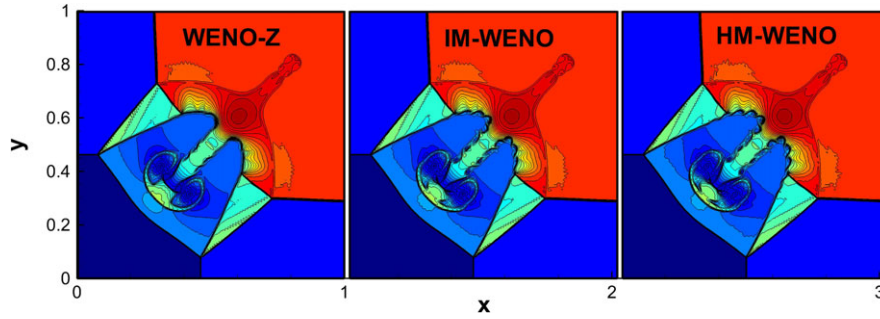


FIGURE 10 Two-dimensional Riemann problem, $N_x \times N_y = 400 \times 400$, 25 contours from 0.2 to 1.85 [Colour figure can be viewed at wileyonlinelibrary.com]

4.5.2 | 2D Riemann problem

The initial conditions of this problem^{19,29} are

$$(\rho, u, v, p) = \begin{cases} (1.5, 0, 0, 1.5), & 0.8 \leq x \leq 1, 0.8 \leq y \leq 1 \\ (0.5323, 1.206, 0, 0.3), & 0 \leq x < 0.8, 0.8 \leq y \leq 1 \\ (0.138, 1.206, 1.206, 0.029), & 0 \leq x < 0.8, 0 \leq y < 0.8 \\ (0.5323, 0, 1.206, 0.3), & 0.8 \leq x \leq 1, 0 \leq y < 0.8, \end{cases} \quad (72)$$

with Dirichlet boundary conditions. The computational domain is $[0, 1] \times [0, 1]$. Figure 10 gives the density contours with $N_x \times N_y = 400 \times 400$ at $t = 0.8$. It can be found that all schemes can capture reflection shocks and contact discontinuities well. Comparing the structures caused by Kelvin-Helmholtz instabilities, it can be seen that HM-WENO generates richer structures than IM-WENO and WENO-Z, which means the new scheme has less numerical dissipation near contact interfaces.

4.5.3 | Double Mach reflection problem

This problem is proposed by Woodward and Colella³⁰ and describes the reflection of a planar Mach shock in air hitting a wedge. The initial conditions of this problem are

$$(\rho, u, v, p) = \begin{cases} (8, 8.25 \cos \frac{\pi}{6}, -8.25 \sin \frac{\pi}{6}, 116.5), & x < \frac{1}{6} + \frac{y}{\sqrt{3}} \\ (1.4, 0, 0, 1.0), & x \geq \frac{1}{6} + \frac{y}{\sqrt{3}}. \end{cases} \quad (73)$$

The computational domain is $[0, 4] \times [0, 1]$. For the bottom boundary, the exact post-shock condition is imposed for the interval $[0, 0.6]$, and a reflective boundary condition is used for the rest. The top boundary is set to describe the exact motion of a Mach 10 shock. Inflow and outflow boundary conditions are used for the left and right boundaries, respectively. Figure 11 gives the density contours with $N_x \times N_y = 960 \times 240$ at $t = 0.2$. Meanwhile, the magnification of the blow-up region around the double Mach stems of each plot is also shown in the picture. It can be found that all schemes can capture shock structures well. However, from three enlarged plots, we can see that the HM-WENO scheme resolves more instability structures than the other two schemes.

4.5.4 | Forward-facing step problem

This problem is also originally from the work of Woodward and Colella.³⁰ The setup of the problem is as follows: the wind tunnel spans a domain of $[0, 3] \times [0, 1]$. A forward-facing step is located at $(0.6, 0.2)$. The problem is initialized by a right-going Mach 3 flow with a density of 1.4 and a pressure of unity. Reflective boundary conditions are applied along the walls of the tunnel. Inflow and outflow boundary conditions are used for the left and right boundaries, respectively. The density contours with $N_x \times N_y = 600 \times 200$ at $t = 4$ is shown in Figure 12. All the schemes perform well with good resolution. Carefully comparing these figures, it can be observed that the roll-up of the vortex sheet captured by HM-WENO is more clear than the others.

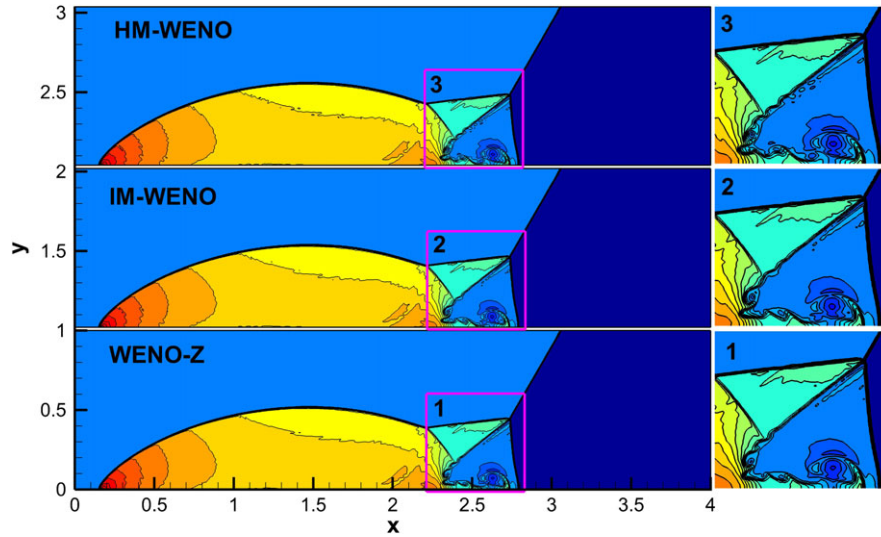


FIGURE 11 Double Mach reflection problem, $N_x \times N_y = 960 \times 240$, 30 contours from 1.2 to 24 [Colour figure can be viewed at wileyonlinelibrary.com]

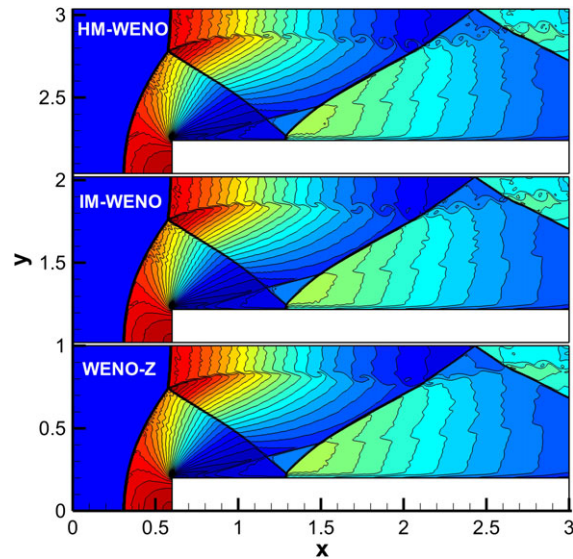


FIGURE 12 Forward-facing step problem, $N_x \times N_y = 600 \times 200$, 30 contours from 0.3 to 6.4 [Colour figure can be viewed at wileyonlinelibrary.com]

4.5.5 | 2D Sedov blast wave problem

The 2D Sedov blast wave problem,^{31,32} which has an exact self-similar solution, is a well-known benchmark test to study a strong explosion problem. The initial conditions of this problem are

$$(\rho, u, v, p) = \begin{cases} (1, 0, 0, 10^{-12}), & \text{if } x > \Delta x, y > \Delta y \\ (1, 0, 0, \frac{0.244816}{\Delta x \Delta y}), & \text{else.} \end{cases} \quad (74)$$

The computational domain is $[0, 1.1] \times [0, 1.1]$. Reflective boundary conditions are applied along the bottom and left boundaries and the outflow conditions are imposed on the top and right boundaries. Figure 13A gives the density contours calculated by HM-WENO with $N_x \times N_y = 160 \times 160$ at $t = 1$, and the density profile along $y = 0$ is shown in Figure 13B. The exact solution is specified in the work of Sedov.³¹ Numerical simulations show that all three schemes can solve this problem. It also can be found that, from the density distribution shown in Figure 13B, HM-WENO can still improve the solution near strong shock wave.

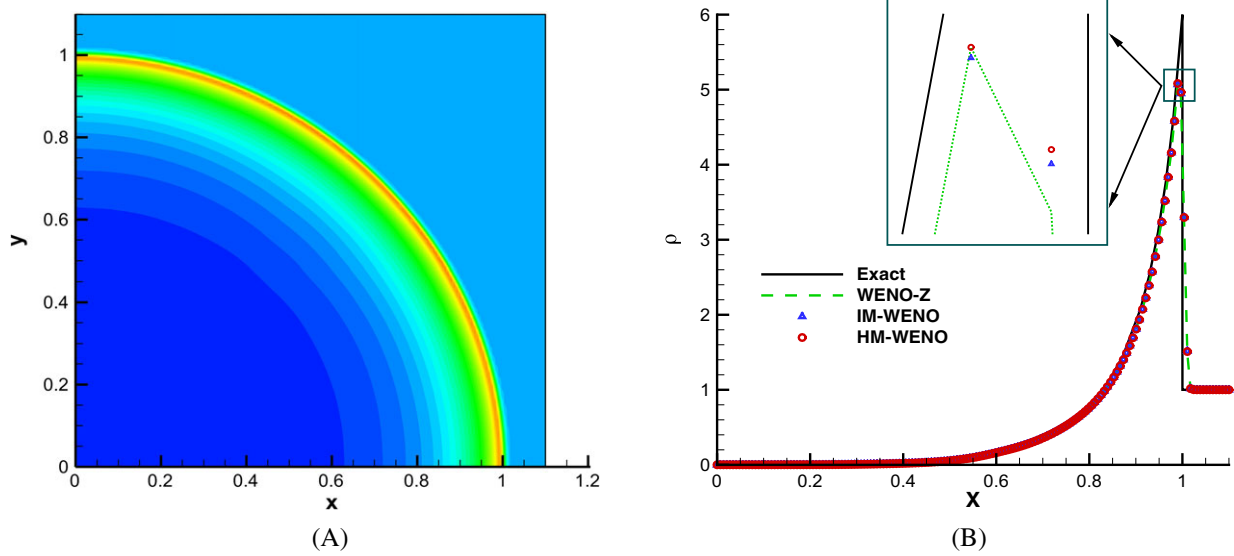


FIGURE 13 2D Sedov blast wave problem: A, Contour of density; B, Density distribution along $y = 0$ [Colour figure can be viewed at wileyonlinelibrary.com]

4.6 | Shock wave impingement on a spatially evolving mixing layer

This problem describes an oblique shock with angle $\beta = 12^\circ$ impacts on a Mach number of 0.6 shear layer and is reflected by a wall at the lower boundary.³³ The governing equation of this problem is 2D Navier-Stokes equations and is given by

$$\frac{\partial U}{\partial t} + \frac{\partial F}{\partial x} + \frac{\partial G}{\partial y} = \frac{1}{Re} \left(\frac{\partial F_v}{\partial x} + \frac{\partial G_v}{\partial y} \right), \quad (75)$$

where U, F, G , vectors are the same as given in Equation (68), and F_v, G_v vectors are given by

$$F_v = \begin{bmatrix} 0 \\ \tau_{xx} \\ \tau_{xy} \\ u\tau_{xx} + v\tau_{xy} + q_x \end{bmatrix}, \quad G_v = \begin{bmatrix} 0 \\ \tau_{yx} \\ \tau_{yy} \\ u\tau_{yx} + v\tau_{yy} + q_y \end{bmatrix}, \quad (76)$$

in which

$$\tau_{xx} = \mu \left(\frac{4}{3} \frac{\partial u}{\partial x} - \frac{2}{3} \frac{\partial v}{\partial y} \right), \quad \tau_{xy} = \tau_{yx} = \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right), \quad \tau_{yy} = \mu \left(\frac{4}{3} \frac{\partial v}{\partial y} - \frac{2}{3} \frac{\partial u}{\partial x} \right),$$

$$q_x = \mu \frac{1}{(\gamma - 1)M^2 Pr} \frac{\partial T}{\partial x}, \quad q_y = \mu \frac{1}{(\gamma - 1)M^2 Pr} \frac{\partial T}{\partial y}.$$

The computational domain is $[0, 200] \times [-20, 20]$. The inflow is specified as

$$u = 2.5 + 0.5 \tan h(2y).$$

For the upper stream inflow ($y > 0$), $\rho_u = 1.6374, p_u = 0.3327$; and for the lower stream inflow ($y < 0$), $\rho_l = 0.3626, p_l = 0.3327$. The upper boundary is set as post-shock wave conditions, and a slip wall condition is applied at the lower wall boundary. Fluctuations are added to the vertical velocity component as

$$v' = \sum_{k=1}^2 a_k \cos(2\pi kt/T + \phi_k) \exp(-y^2/b),$$

in which $b = 10, a_1 = a_2 = 0.05, \phi_1 = 0, \phi_2 = \pi/2, T = \lambda/u_c, \lambda = 30, u_c = 2.68$. The Prandtl number Pr is set to 0.72, and the Reynolds number Re is chosen to be 500. The Steger-Warming flux splitting method²⁶ and WENO reconstruction for each component of split fluxes are also used for the inviscid convective fluxes, and the viscous terms are discretized with the fourth-order central difference scheme. Figure 14 gives the density contours with $N_x \times N_y = 320 \times 80$ at $t = 120$. An apparent difference is that, in the region of $x > 120$, the present scheme obtains more clear vortex structures than the WENO-Z and IM-WENO schemes.

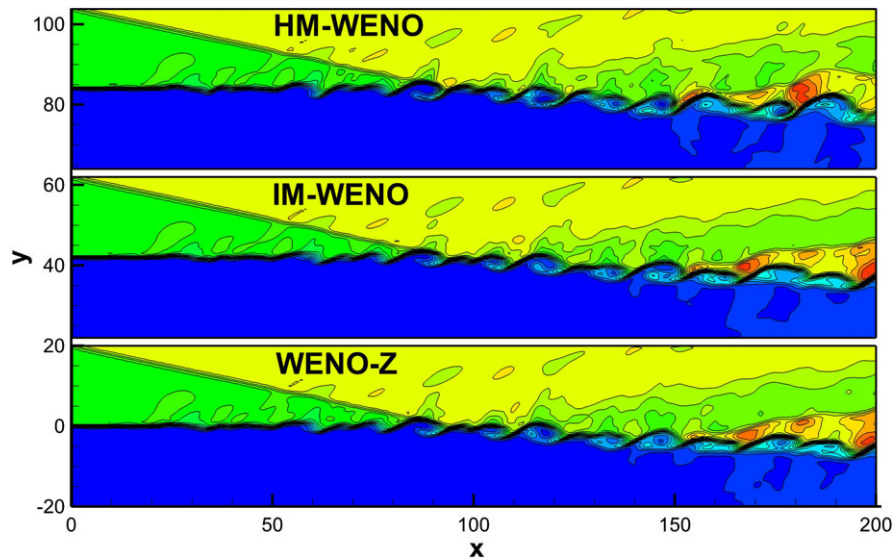


FIGURE 14 Shock/shear layer interaction problem, $N_x \times N_y = 320 \times 80$, 20 contours from 0.5 to 2.7 [Colour figure can be viewed at wileyonlinelibrary.com]

5 | CONCLUSION REMARKS

This paper analyzes the reason of several WENO schemes that failed to decrease the numerical dissipation near discontinuities. Then, a high performance fifth-order multistep WENO scheme is proposed by using a nonlinear function of two adjacent local smoothness indicators to replace previous linear combination. The function makes the calculated weights more accurate approximating to the ideal intermediate weights and, hence, decreases the numerical dissipation at transition points. The new scheme has the similar formula as those of the improved multistep WENO scheme suggested by Ma et al.¹⁹; hence the resulted scheme is also more efficient than the original multistep WENO scheme of Shen et al.¹⁶ Meanwhile, theoretical analysis shows that the new scheme can improve the accuracy at transition points without reducing the accuracy in smooth regions including critical points. Various numerical examples are presented to demonstrate the high performance of the new scheme, such as the efficiency, the robustness, the high resolution of discontinuities, and the fifth-order accuracy in smooth regions.

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APPENDIX

The process for analyzing the accuracy of the IM-WENO and HM-WENO schemes in smooth regions including critical points is presented here, where the symbols p and m represent $+$ and $-$, respectively.

$$\begin{aligned}
 &> p\beta_{00} := \frac{1}{4}(f(-2dx) - 4f(-dx) + 3f(0))^2 + \frac{13}{12}(f(-2dx) - 2f(-dx) + f(0))^2 \\
 &> p\beta_{01} := \frac{1}{4}(f(-dx) - f(dx))^2 + \frac{13}{12}(f(-dx) - 2f(0) + f(dx))^2 \\
 &> p\beta_{02} := \frac{1}{4}(3f(0) - 4f(dx) + f(2dx))^2 + \frac{13}{12}(f(0) - 2f(dx) + f(2dx))^2 \\
 &> h(p\beta_{00}, p\beta_{01}) := 2p\beta_{00} + \left(\frac{p\beta_{00} - p\beta_{01}}{p\beta_{00} + p\beta_{01}}\right)^2 p\beta_{01} \quad \# \text{ For the IM-WENO scheme : } h(p\beta_{00}, p\beta_{01}) := p\beta_{00} + p\beta_{01} \\
 &> h(p\beta_{02}, p\beta_{01}) := 2p\beta_{02} + \left(\frac{p\beta_{02} - p\beta_{01}}{p\beta_{02} + p\beta_{01}}\right)^2 p\beta_{01} \quad \# \text{ For the IM-WENO scheme : } h(p\beta_{02}, p\beta_{01}) := p\beta_{02} + p\beta_{01} \\
 &> p\beta_{01} := \frac{h(p\beta_{00}, p\beta_{01})h(p\beta_{02}, p\beta_{01})}{h(p\beta_{00}, p\beta_{01}) + h(p\beta_{02}, p\beta_{01})} \\
 &> m\beta_{00} := \frac{1}{4}(f(-3dx) - 4f(-2dx) + 3f(-dx))^2 + \frac{13}{12}(f(-3dx) - 2f(-2dx) + f(-dx))^2 \\
 &> m\beta_{01} := \frac{1}{4}(f(-2dx) - f(0))^2 + \frac{13}{12}(f(-2dx) - 2f(-dx) + f(0))^2 \\
 &> m\beta_{02} := \frac{1}{4}(3f(-dx) - 4f(0) + f(dx))^2 + \frac{13}{12}(f(-dx) - 2f(0) + f(dx))^2 \\
 &> h(m\beta_{00}, m\beta_{01}) := 2m\beta_{00} + \left(\frac{m\beta_{00} - m\beta_{01}}{m\beta_{00} + m\beta_{01}}\right)^2 m\beta_{01} \quad \# \text{ For the IM-WENO scheme : } h(m\beta_{00}, m\beta_{01}) := m\beta_{00} + m\beta_{01} \\
 &> h(m\beta_{02}, m\beta_{01}) := 2m\beta_{02} + \left(\frac{m\beta_{02} - m\beta_{01}}{m\beta_{02} + m\beta_{01}}\right)^2 m\beta_{01} \quad \# \text{ For the IM-WENO scheme : } h(m\beta_{02}, m\beta_{01}) := m\beta_{02} + m\beta_{01} \\
 &> m\beta_{01} := \frac{h(m\beta_{00}, m\beta_{01})h(m\beta_{02}, m\beta_{01})}{h(m\beta_{00}, m\beta_{01}) + h(m\beta_{02}, m\beta_{01})} \\
 &> p\tau_{05} := p\beta_{02} - p\beta_{00} \\
 &> m\tau_{05} := m\beta_{02} - m\beta_{00} \\
 &> D_p := p\beta_{00} * p\beta_{01} * p\beta_{02} + p\tau_{05} * p\beta_{00} * p\beta_{01} * p\beta_{02} * \left(\frac{1}{10p\beta_{00}} + \frac{6}{10p\beta_{01}} + \frac{3}{10p\beta_{02}}\right) \\
 &> D_m := m\beta_{00} * m\beta_{01} * m\beta_{02} + m\tau_{05} * m\beta_{00} * m\beta_{01} * m\beta_{02} * \left(\frac{1}{10m\beta_{00}} + \frac{6}{10m\beta_{01}} + \frac{3}{10m\beta_{02}}\right) \\
 &> D(f)(0) := 0 \\
 &> series(D_p * D_m, dx = 0) \\
 &> N_m := m\tau_{05} * m\beta_{00} * m\beta_{01} * m\beta_{02} * \left(-\frac{1}{4} \frac{1}{10m\beta_{00}} + \frac{1}{12} \frac{6}{10m\beta_{01}} - \frac{1}{12} \frac{3}{10m\beta_{02}}\right) D^{(3)}(f) \left(-\frac{dx}{2}\right) \\
 &> N_p := p\tau_{05} * p\beta_{00} * p\beta_{01} * p\beta_{02} * \left(-\frac{1}{4} \frac{1}{10p\beta_{00}} + \frac{1}{12} \frac{6}{10p\beta_{01}} - \frac{1}{12} \frac{3}{10p\beta_{02}}\right) D^{(3)}(f) \left(-\frac{dx}{2}\right) \\
 &> series(D_m * N_p - D_p * N_m, dx = 0) \\
 &\hspace{15em} O(dx^{27})
 \end{aligned}$$