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# Simultaneously achieving strength and ductility in Ni<sub>3</sub>Al nanowires with superlattice intrinsic stacking faults

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## ABSTRACT

Simultaneously improving strength and ductility has been an attractive theme in materials science and engineering. Through designing nanostructures, it is possible to overcome the traditional trade-off between ductility and strength of materials. In this paper, we show that introducing superlattice intrinsic stacking faults in nickel aluminide (Ni<sub>3</sub>Al) can facilitate its strength and toughness. In comparison with twin boundaries, the enhancing effect of superlattice intrinsic stacking faults is more obvious. Most significantly, the yield strength of samples with superlattice intrinsic stacking faults is always superior to their single crystalline counterparts, indicating that the yield strength of single crystalline Ni<sub>3</sub>Al can be exceeded. These findings provide new insights into the nanostructural design of aerospace materials.

## 1. Introduction

Nanostructured metallic materials with ultrafine-grained, heterogeneous and even defective structures show exceptional mechanical properties such as superior strength, which are very promising in various applications. However, super-strong metallic nanomaterials usually have a low ductility at ambient temperature, which significantly restricts their wide usage [1]. Nevertheless, several nanostructured metals and alloys have been found to exhibit a concurrent high strength and good ductility, including nanostructured twinning, gradient-structured and heterogeneous lamella materials [2–4] as well as other types of hetero-structured materials [5,6]. It has shown that planar defects of twin boundary (TB) can simultaneously enhance strength and ductility of nanostructured face-centered-cubic (FCC) metallic materials [2,7–9].

Because of low stacking faults energy in FCC metals, there are a large number of stacking faults generated during plastic deformation via slip of partial dislocations or dissociation of full dislocations. Here, it is worth noting that, similar to TBs, stacking faults are a kind of planar defects. However, there is lack of progress on how stacking faults affect

strength and ductility of nanostructured FCC metals. This is mainly due to the difficulty of differentiating individual contributions in FCC metals, since formation of stacking faults is accompanied with deformation twins. Therefore, the observed mechanical behaviors are usually attributed to TBs [8,9]. Whereas stacking faults should in no doubt have a positive impact on strength and ductility of nanostructured FCC metals and alloys. For example, stacking faults can effectively increase the strength of FCC structural materials such as Ag and Au [10]. Moreover, the effect of stacking faults on strength and ductility was obviously observed in nanostructured hexagonal close packed metals and alloys [11–13]. As discovered in nanostructured Mg alloy, stacking faults are effective on blocking and accumulating dislocations, which plays a similar role as TBs. Consequently, the high density of stacking faults produces high strength and good ductility. In addition, the strengthening effect of stacking faults was also demonstrated in brittle materials, such as gallium arsenide semiconductor nanowires [14] and silicon carbide ceramic nanorods [10]. That is, similar to TBs, the influence of stacking faults on the mechanical properties and deformation mechanism is closely related to the interaction between dislocations and stacking faults. However, there has been no systematic research aiming

*Abbreviations:* CSF, Complex stacking fault; FCC, Face-centered-cubic; Ni<sub>3</sub>Al, Nickel aluminide; SC, Single crystal; SISF, Superlattice intrinsic stacking fault; TB, Twin boundary.

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at the effect of stacking faults on strength and ductility of FCC materials.

Ni<sub>3</sub>Al is an intermetallic ordered alloy with the L1<sub>2</sub> structure, where Al atoms occupy corners and Ni atoms take over face centers of an FCC cell. Due to its potential corrosion, oxidation and creep resistance, high strength and good thermal properties, Ni<sub>3</sub>Al has been widely applied in aerospace industries such as turbine blades and vanes in aircraft engines [15–19]. Extensive experimental and theoretical efforts have been made to elucidate the structural and mechanical properties of single crystal Ni<sub>3</sub>Al (SC-Ni<sub>3</sub>Al) [20]. However, the low susceptibility to plastic deformation and the high tendency to brittle cracking strongly limit their industrial applications [21]. Through nanostructural design, some metallic materials can achieve strengthening and toughening [22–25]. For instance, Wang et al. [26] investigated plastic deformation and failure mechanisms of Ni<sub>3</sub>Al nanowires with TBs (TB-Ni<sub>3</sub>Al). Their results indicated that strength, ductility and fracture toughness of TB-Ni<sub>3</sub>Al increase simultaneously with reducing the spacing between neighboring TBs.

The super-lattice structure of Ni<sub>3</sub>Al increases the complexities of microstructures and consequently, the modes of deformation. Depending on the diversities of dislocation reactions, there are kinds of stable stacking faults in Ni<sub>3</sub>Al, e.g., superlattice intrinsic stacking fault (SISF), antiphase boundary and complex stacking fault (CSF) [27,28]. For deformation in Ni<sub>3</sub>Al, one stable dissociation of dislocations is that a  $\langle 110 \rangle$  super-dislocation dissociates into two  $1/2\langle 110 \rangle$  super-partial dislocations bounding with an antiphase boundary on (111) and (010) planes, respectively. The other stable dissociation of the  $\langle 110 \rangle$  super-dislocation also generates two  $1/3\langle 112 \rangle$  Shockley super-partial dislocations bounding with an SISF. The metastable dissociation of a  $\langle 110 \rangle$  super-dislocation brings one  $1/2\langle 110 \rangle$  super-partial and two  $1/6\langle 112 \rangle$  Shockley partials bounding with a CSF. In addition, the structure of TBs can also be considered as ‘thick’ stable stacking faults. Studying these stacking faults is pivotal to a better understanding of strength and ductility of nanostructured Ni<sub>3</sub>Al. Here, the size of stacking faults plays a major role in dislocation mobility, which drastically affects the mechanical properties of Ni<sub>3</sub>Al. However, previous studies are mainly concentrated on the energy of stacking faults in nanostructured

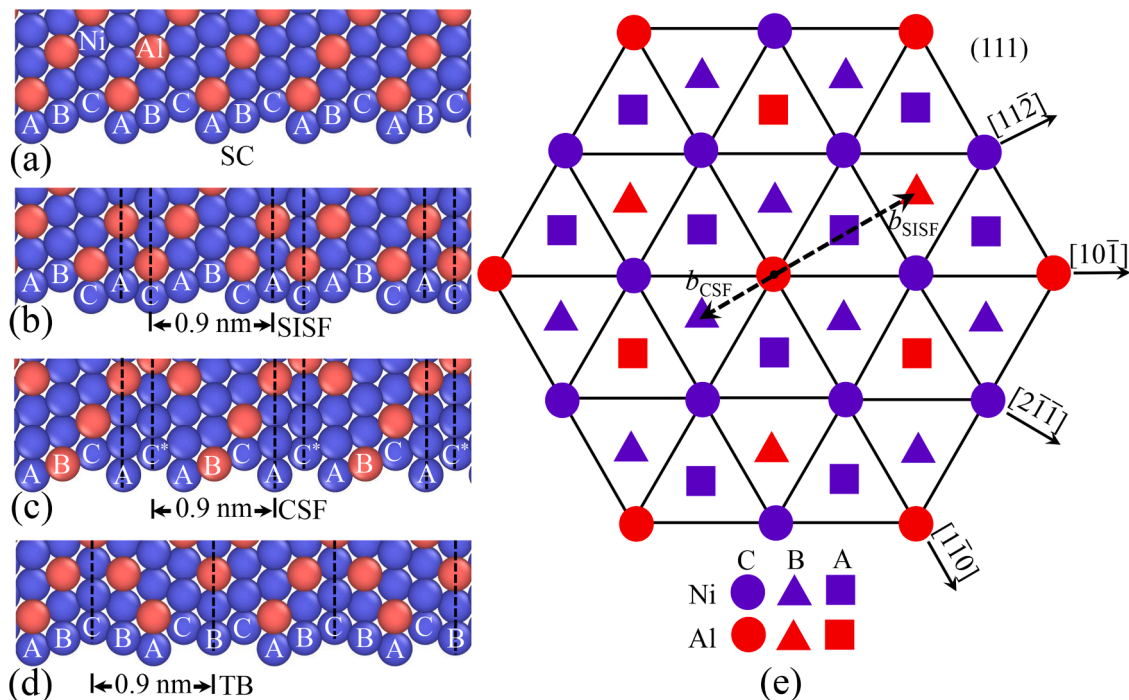
Ni<sub>3</sub>Al by first-principles calculations [27,28]. In contrast, there are relatively few investigations in molecular dynamics simulations, which can establish an all-atom model to examine the mechanical properties of nanostructured Ni<sub>3</sub>Al nanowires.

In this paper, stacking faults are introduced into Ni<sub>3</sub>Al to investigate whether their configurations could strengthen and toughen Ni<sub>3</sub>Al nanowire in comparison with nanoscale TBs. By using molecular dynamics simulations, a series of SC-Ni<sub>3</sub>Al, CSF-Ni<sub>3</sub>Al, SISF-Ni<sub>3</sub>Al and TB-Ni<sub>3</sub>Al nanowires under uniaxial tension have been modeled with various spacings between the planar defects. Numerical results are discussed in terms of their stress-strain curves, Young’s modulus, yield strength, and the corresponding uniform elongation, i.e., strain at which necking occurs during a tensile process.

## 2. Numerical models and methodology

### 2.1. Nanostructured Ni<sub>3</sub>Al models

Based on the stacking sequences of SC-, CSF-, SISF- and TB-Ni<sub>3</sub>Al as illustrated in Fig. 1 a–d, models can be established on the fact that Ni<sub>3</sub>Al adopts a close-packed structure with an arrangement of three successive planes, denoting as A, B and C, along the [111] direction (see Fig. 1e). Here, SC-Ni<sub>3</sub>Al is built up according to the L1<sub>2</sub> crystal structure with periodic repeat of the ABC stacking sequence. CSF-Ni<sub>3</sub>Al and SISF-Ni<sub>3</sub>Al models are formed by shearing C with  $a/6[11\bar{2}]$  (111) and  $a/3[11\bar{2}]$  (111), respectively [27], with a lattice constant of Ni<sub>3</sub>Al. An SISF-Ni<sub>3</sub>Al with a spacing of 0.9 nm between parallel SISFs corresponds to a stacking sequence of ABCAC as a periodically repeating unit, where bold and italic letters represent planar defects. Whereas a CSF-Ni<sub>3</sub>Al with the same spacing between parallel CSFs consists of a stacking sequence of ABCAC\* as a periodic unit. Here, the C\* layer adopts an alternative arrangement of atoms in contrast to that of C layer in an SISF-Ni<sub>3</sub>Al [27]. The corresponding unit of a periodically stacking sequence of TB-Ni<sub>3</sub>Al is CBACBCAB, with a spacing of 0.9 nm between parallel TBs. These planar defects of Ni<sub>3</sub>Al were characterized through the experimental observation with a transmission electron microscopy [29,30], indicating



**Fig. 1.** The stacking sequence of nanostructured L1<sub>2</sub> Ni<sub>3</sub>Al with (a) SC, (b) SISF, (c) CSF and (d) TB with a spacing of 0.9 nm between parallel planar defects. (e) The atomic arrangement of L1<sub>2</sub> structure in top view. A, B and C represent close-packed sites. Operation with the vectors  $b_{\text{SISF}}$  and  $b_{\text{CSF}}$  generates SISF and CSF, respectively.

that the intrinsic planar defects play an important role in the plastic deformation processes of Ni-based superalloys.

The typical models of nanostructured Ni<sub>3</sub>Al are sketched in Fig. 2, including CSF, SISF and TB models with a spacing of 0.9 nm between planar defects. All these wires were created in a cylindrical lateral shape with an aspect ratio of length ( $L$ ) to diameter ( $D = 6$  nm) at least larger than 3.0. Spacing between planar defects varies from 0.9 nm (i.e., the smallest spacing to ensure a complete ABC stacking sequence of L1<sub>2</sub> structure along the [111] direction) to 10.7 nm. In order to show the changing tendency of yield strength, uniform elongation and Young's modulus versus spacing, five simulations were performed for each spacing. An SC nanowire was taken as a reference to investigate the strengthening and toughening effect of TBs, SISFs and CSFs. Each model contains up to ~80,000 atoms, depending on the length of a nanowire.

## 2.2. Molecular dynamics simulation

Atomistic simulations were performed by using the Largescale Atomic/Molecular Massively Parallel Simulator [31]. An embedded-atom method potential function for the Ni-Al system developed by Mishin [32] was taken to describe the atomic interaction in Ni<sub>3</sub>Al. In this function, the total energy,  $E$ , of a system is depicted as

$$E = \sum_{\substack{i,j \\ i \neq j}} V_{EAM}(r_{ij}) + \sum_i F(\bar{\rho}_i), \quad (1)$$

where  $V_{EAM}(r_{ij})$ , a pair potential, is a function of the distance  $r_{ij}$  between atoms  $i$  and  $j$ . Moreover,  $F$  is the embedding energy of atom  $i$ , and  $\bar{\rho}_i$  is the electron density, which is written as

$$\bar{\rho}_i = \sum_{j \neq i} g_j(r_{ij}), \quad (2)$$

where  $g_j(r_{ij})$  is the electron density of atom  $j$ .

Such a potential was built up by fitting to data of both experiments and first-principles. It can depict an accurate lattice, the mechanical properties, and especially energetics of point defects and planar faults. The latter is essential to study planar faults dominated deformation mechanisms of Ni<sub>3</sub>Al [33].

Periodic boundary conditions were introduced in the Z-[111] crystalline directions. Simulations were performed by integrating Newton's equations of motion for all atoms with a time step of 1 fs. At the beginning of simulation, Ni<sub>3</sub>Al nanowires were energetically minimized by relaxing a sample for 100 ps at 300 K. To obtain the mechanical properties, a uniaxial tensile load along the [111] direction (perpendicular to planes of CSFs, SISFs and TBs) was applied with a constant strain rate of  $5 \times 10^8 \text{ s}^{-1}$ . Stress in a stress-strain relationship was calculated by the Virial scheme, which was usually used in atomistic simulations [34–37]. Young's modulus was fitted from the ~2% elastic regime of a stress-strain curve. During uniaxial loading, transverse directions were permitted to relax and kept a stress-free condition. Deformation and defects of Ni<sub>3</sub>Al nanowires were recognized by common neighbor and dislocation analysis and then, visualized by the software OVITO [38].

## 3. Simulation results

### 3.1. Tensile stress-strain relationships

As shown in Fig. 3a, all stress-strain curves of Ni<sub>3</sub>Al nanowires linearly rise in stress with the increase of strain until their yield strength. After that, stress encounters a sudden drop and then undergoes fluctuation with further increasing strain. However, these four curves do not synchronize. Specifically, the SISF-Ni<sub>3</sub>Al nanowire yields the biggest yield strength of 17.2 GPa, whilst the CSF-Ni<sub>3</sub>Al nanowire generates the smallest yield strength of 15.2 GPa. Between them, TB-Ni<sub>3</sub>Al has bigger yield strength (16.4 GPa) than that of CSF-Ni<sub>3</sub>Al, but it is still less than

that (16.9 GPa) of SC-Ni<sub>3</sub>Al. The uniform elongation of four nanowires keeps step with their corresponding yield strength, with values of 7.98%, 7.53%, 7.18% and 6.88% for SISF-, SC-, TB- and CSF-Ni<sub>3</sub>Al, respectively.

Real-time detection on dislocation activities indicates that the stress-strain curves closely relate to their densities of dislocation lines (see Fig. 3b). Taking the CSF-Ni<sub>3</sub>Al nanowire as an example, the first dislocation event (i.e., dislocation nucleation) is captured as yield strength is arrived. Then, the density of dislocation lines rapidly increases to its maximum value of  $1.5 \times 10^{-3} \text{ \AA}^{-2}$  at the strain of 6.63%. This period echoes exactly to a sudden drop in stress from its peak value to 7.2 GPa. After that, the density of dislocation lines gradually reduces, corresponding to fluctuation of stress with the increase of strain. The highest density ( $2.7 \times 10^{-3} \text{ \AA}^{-2}$ ) of dislocation lines appears in the SISF-Ni<sub>3</sub>Al nanowire at a strain of 7.63%. The SC-Ni<sub>3</sub>Al nanowire, however, produces the lowest density of dislocation lines ( $1.4 \times 10^{-3} \text{ \AA}^{-2}$ ) as strain reaches 7.48%. The TB-Ni<sub>3</sub>Al nanowire is the second one to attain its maximum value of density of dislocation lines ( $2.3 \times 10^{-3} \text{ \AA}^{-2}$ ) with a strain at 7.28%.

### 3.2. Deformation mechanisms of SC-Ni<sub>3</sub>Al and TB-Ni<sub>3</sub>Al

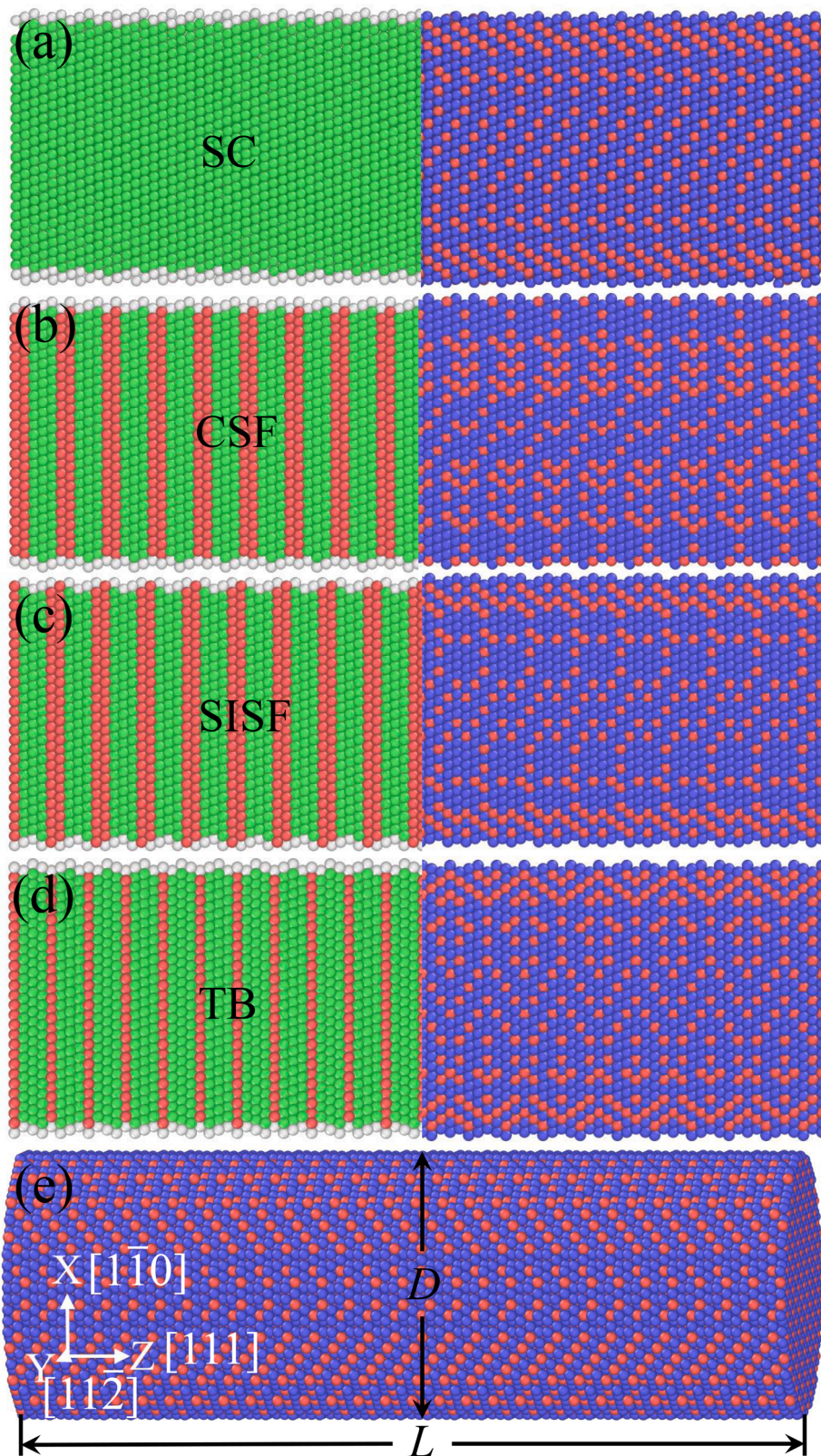
As seen in Fig. 4, as strain is less than 6.98%, there are no dislocations in the SC-Ni<sub>3</sub>Al nanowire, declaring elastic deformation of it (Fig. 4a). Then, with strain increasing, a  $1/6\langle 112 \rangle$  Shockley dislocation nucleates on surface of the nanowire and propagates inward, forming a layer of tilted stacking faults behind it (Fig. 4b). As more  $1/6\langle 112 \rangle$  Shockley dislocations continuously nucleate and spread inside the nanowire, they meet to form a  $1/6\langle 110 \rangle$  stair-rod dislocation at their junction area (Fig. 4c). Finally, as illustrated in Fig. 4d, when strain reaches 14.98%, the dislocation density falls to its minimum due to annihilation of dislocations on surface of the nanowire. This can be postponed by introducing planar defects such as SISFs and TBs. Residual dislocations in the deformed nanowire are mainly  $1/6\langle 112 \rangle$  Shockley type, accompanied by multiple tilted stacking faults.

In contrast to that in the SC-Ni<sub>3</sub>Al nanowire, dislocations first nucleate on surface of a TB-Ni<sub>3</sub>Al nanowire adjacent to a TB and then spread inward at a strain of 6.88% (Fig. 5a). As dislocations move to a TB, they are impeded and react with TB. Reaction brings  $1/6\langle 110 \rangle$  stair-rod and  $1/3\langle 111 \rangle$  Frank dislocations, accounting for the density of dislocation lines of 8.00% and 8.60%, respectively. Reaction also sets off migration and detwinning of TB as shown in Fig. 5b. With strain increasing to 7.23%, TB migrates downward and the pinning effect is observed above it. Dislocations participating pinning are mainly  $1/6\langle 112 \rangle$  (69.70%) and a small amount of  $1/6\langle 110 \rangle$  stair-rod,  $1/3\langle 100 \rangle$  Hirth, and  $1/2\langle 110 \rangle$  perfect (see Fig. 5c). Consequently, necking happens at the site of TB. Further increase in strain induces serious necking and more pinning events as illustrated in Fig. 5d. It is worth noting that, however, there is no dislocation passing through TBs during stretching of a TB-Ni<sub>3</sub>Al nanowire.

### 3.3. Deformation mechanisms of CSF-Ni<sub>3</sub>Al and SISF-Ni<sub>3</sub>Al

As shown in Fig. 6, at a strain of 6.33%, a  $1/6\langle 112 \rangle$  Shockley dislocation nucleates on surface of nanowire near a CSF, and then, it spreads obliquely inward with a tilted stacking fault left behind it. As it meets the CSF, such a dislocation stimulates a new  $1/6\langle 112 \rangle$  Shockley dislocation on CSF. Finally, with the original dislocation cutting through CSF, the stimulated one spreads transversely along CSF. Transverse propagation of the stimulated  $1/6\langle 112 \rangle$  dislocation causes fading of CSF (see Fig. 6a). As strain reaches 6.48%, the transversely moving dislocation has gone out of surface of the nanowire, resulting in complete fading of CSF on which it once moves. Meanwhile, the original  $1/6\langle 112 \rangle$  dislocation meets another CSF. It induces a new  $1/6\langle 112 \rangle$  dislocation and crosses over CSF to continue its movement. Here, the second generated dislocation propagates obliquely without causing





**Fig. 2.** Tensile models of nanostructured  $\text{Ni}_3\text{Al}$  nanowires, including cross-section diagrams of (a) SC-, (b) CSF-, (c) SISF- and (d) TB- $\text{Ni}_3\text{Al}$  nanowires. Spacing between parallel planar defects is 0.9 nm. To show planar defects, a half nanowire is colored by common neighbor analysis with green and red representing the FCC structure and planar defects. (e) The cylindrical shape of an SC- $\text{Ni}_3\text{Al}$  nanowire with length  $L = 18$  nm and diameter  $D = 6$  nm.



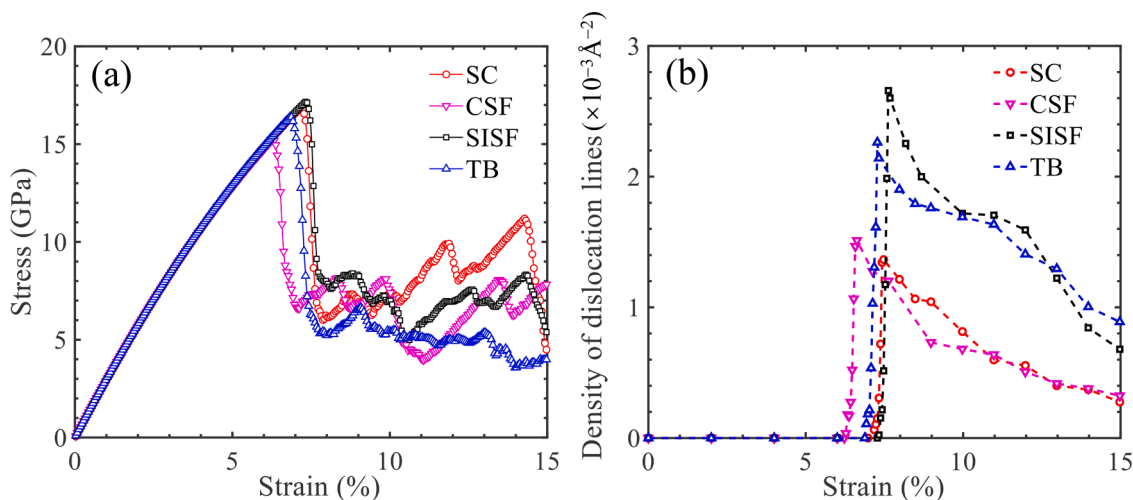


Fig. 3. (a) Typical tensile stress-strain relationships and (b) their corresponding densities of dislocation lines in nanostructured  $\text{Ni}_3\text{Al}$  nanowires with a spacing of 4.5 nm between parallel planar defects.

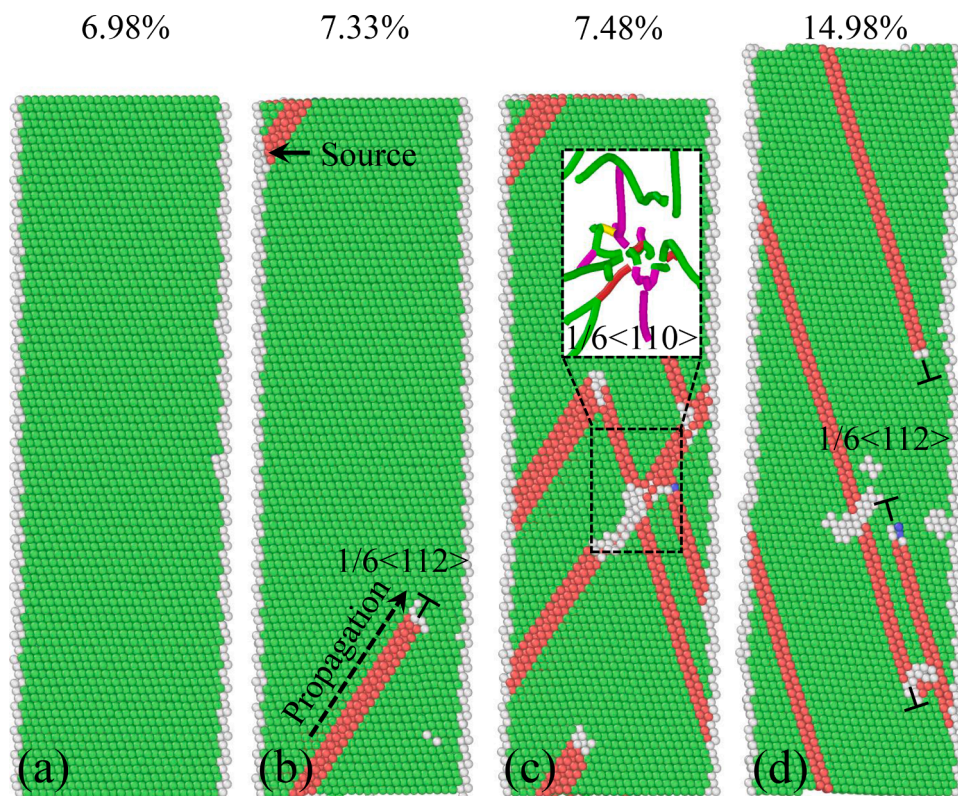


Fig. 4. Atomic configurations of an SC- $\text{Ni}_3\text{Al}$  nanowire with a diameter of 6.0 nm under uniaxial stretching at various tensile strains of (a) 6.98%, (b) 7.33%, (c) 7.48% and (d) 14.98%, where atoms are colored by common neighbor analysis. Inset in (c) shows the structure of local dislocations visualized by dislocation analysis with green, purple, yellow and red lines indicating  $1/6\langle 112 \rangle$  Shockley,  $1/6\langle 110 \rangle$  stair-rod,  $1/3\langle 100 \rangle$  Hirth, and other kind of dislocations, respectively.

fading of CSF (see Fig. 6b). Moreover, more  $1/6\langle 112 \rangle$  dislocations nucleate on surface of the nanowire and moves inward. Further increase in strain induces more dislocation activities as shown in Fig. 6c–e. Detection on dislocation activities also captures other types of dislocations such as  $1/6\langle 110 \rangle$  stair-rod,  $1/3\langle 100 \rangle$  Hirth, and  $1/2\langle 110 \rangle$  perfect (see local enlarged drawings in Fig. 6d and e). However, these dislocations do not contribute to fading of CSFs.

Adjacent to intersections between SISFs and the surface of a nanowire,  $1/6\langle 112 \rangle$  Shockley dislocations nucleate and propagate inward as strain passes by 7.38% (see Fig. 7a). With strain increasing,  $1/$

$6\langle 112 \rangle$  dislocations propagate to encounter SISFs. As they overcome obstacles, new  $1/6\langle 112 \rangle$  dislocations are stimulated at SISFs (Fig. 7b and c). Interaction between an original  $1/6\langle 112 \rangle$  and a new stimulated one near SISFs produces a  $1/6\langle 110 \rangle$  stair-rod on SISFs (see Fig. 7d and e). The  $1/6\langle 110 \rangle$  stair-rod does not propagate and keeps SISFs without fading with the increase of strain. Near SISFs, the  $1/6\langle 110 \rangle$  stair-rod pins other types of dislocations such as  $1/2\langle 110 \rangle$  perfect,  $1/3\langle 100 \rangle$  Hirth, and  $1/6\langle 112 \rangle$  Shockley (amplified regions in Fig. 7d and e). These pinned dislocations consist of 1.20%, 7.80% and 66.70%, respectively, in the density of dislocation lines at a strain of 14.98%.

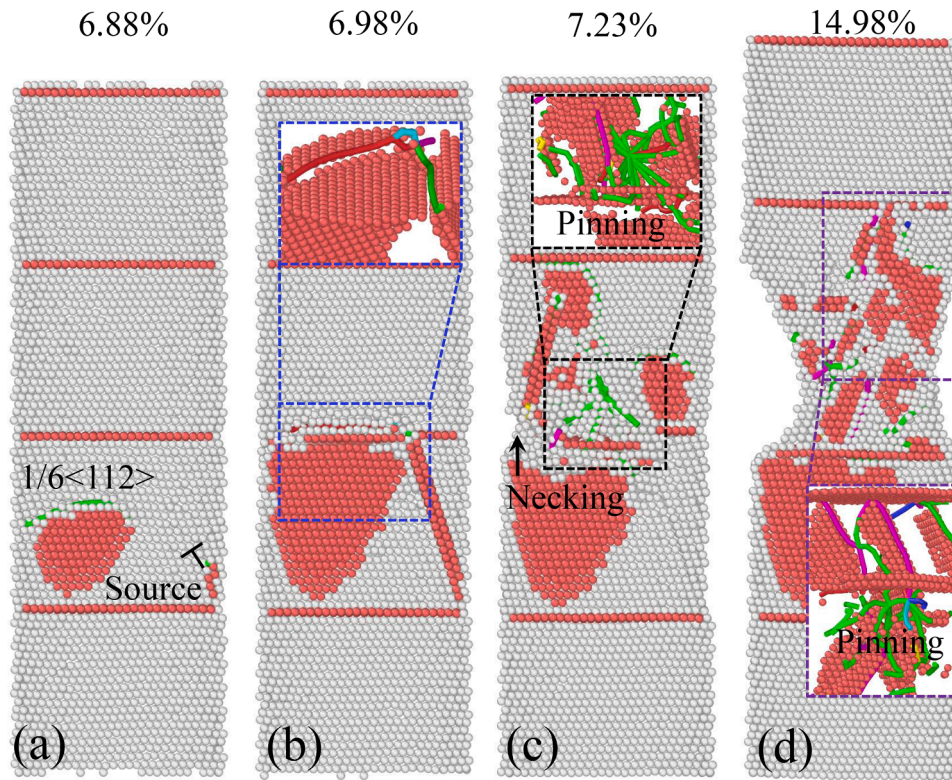


Fig. 5. Atomic configurations of a TB- $\text{Ni}_3\text{Al}$  nanowire with a spacing of 4.5 nm between parallel TBs under uniaxial tension at various strains of (a) 8.38%, (b) 8.53%, (c) 9.98% and (d) 14.98%, where atoms are colored by the dislocation analysis and FCC structures are removed for clarity. Insets in (b–d) show the structures of local dislocations.

### 3.4. Effects of the spacing between planar defects

The mechanical properties of nanostructured  $\text{Ni}_3\text{Al}$  nanowires significantly depend on spacing between planar defects, as summarized in Fig. 8. Strengthening is achieved in SISF- and TB-nanowires. The yield strength of SISF-nanowires increases by 11.3% from 16.8 to 18.7 GPa with spacing between planar defects reducing from 10.7 to 0.9 nm. TB-nanowires brings a 16.0% growth of yield strength from 16.2 to 18.8 GPa at the same spacing range. Both SISF- and TB-nanowires possess an ability to exceed yield strength of an SC-nanowire as spacing between parallel planar defects is reduced less than 4.5 and 2.1 nm for SISF and TB, respectively (see Fig. 8a). The yield strength  $\sigma_Y$  of SISF- and TB- $\text{Ni}_3\text{Al}$  nanowires follows the Hall-Petch relationship, that is

$$\sigma_Y = \sigma_0 + \frac{k}{d^n}, \quad (3)$$

where  $\sigma_0$  and  $k$  are the material and structural dependent parameters,  $d$  is spacing between parallel planar defects, and  $n$  is an exponent. By fitting simulation results of nanowires with a diameter of 6 nm to Eq. (3), the constants  $\sigma_0$  and  $k$  can be determined as 16.4 GPa and  $1.8 \text{ nm}^{-1}$  for SISF- $\text{Ni}_3\text{Al}$  nanowires and 14.6 GPa and  $3.5 \text{ nm}^{-1/2}$  for TB- $\text{Ni}_3\text{Al}$  nanowires, respectively. Variation of the diameter just produces alternative values of  $\sigma_0$  and  $k$  in Eq. (3) since the sample size has been implied within them. Most importantly, the values of  $n$  are 1 and 1/2 for SISF- $\text{Ni}_3\text{Al}$  and TB- $\text{Ni}_3\text{Al}$  nanowires, respectively (see Fig. 8a). Here it is of interest to note that there is no inverse Hall-Petch effect even as spacing between parallel planar defects is cut down to its lower end of 0.9 nm (see Appendix A for the structural evolution of nanowires under uniaxial tension). Fig. 8b further indicates that the uniform elongation of SISF- and TB-nanowires goes beyond that of an SC-nanowire as spacing between planar defects is less than 4.5 and 2.1 nm, respectively. On the contrary, there is no strengthening in CSF-nanowires. Their yield strengths are always lower than that of an SC-nanowire. Moreover,

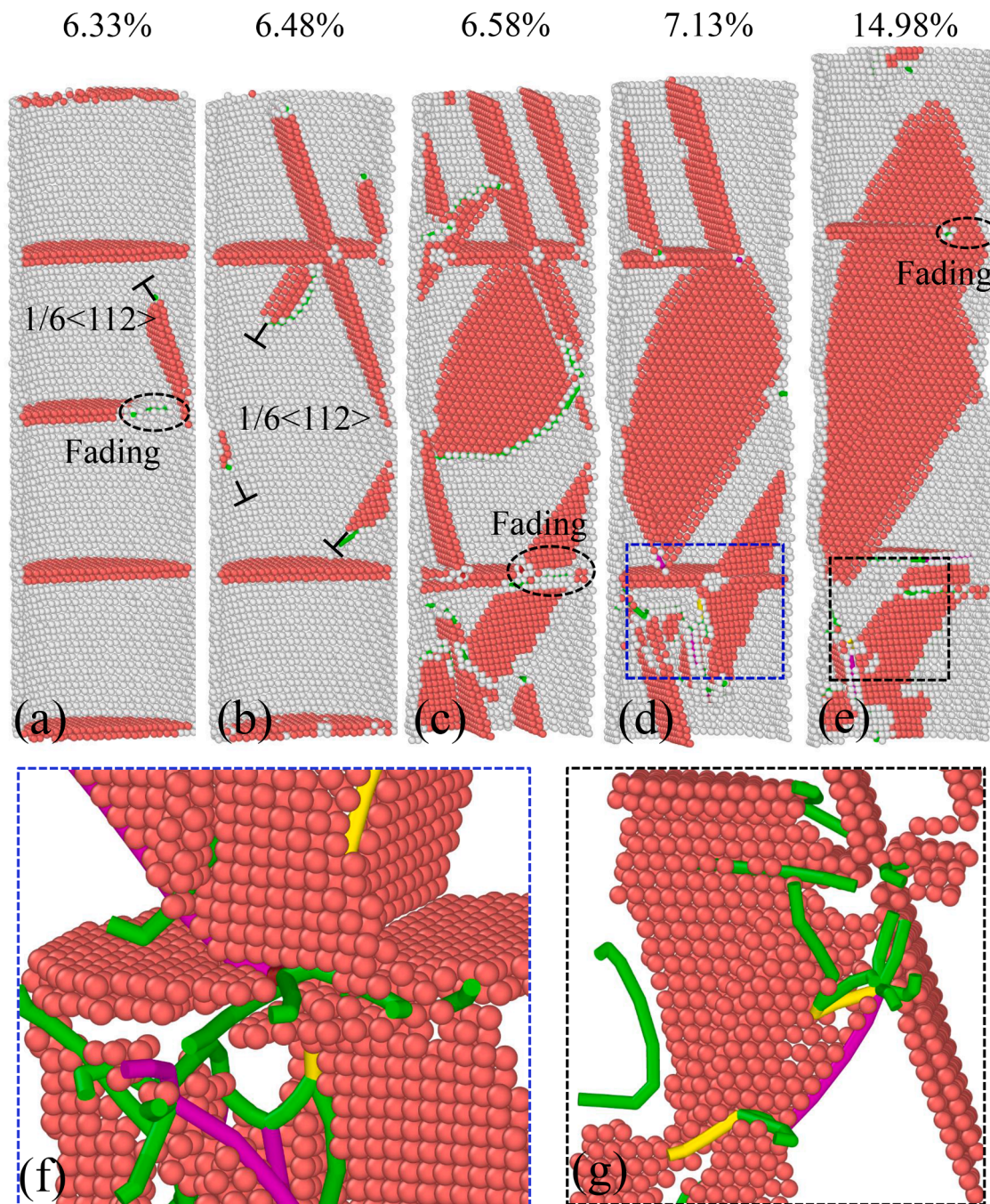
neither the uniform elongation nor Young's modulus of them can compete with that of an SC-nanowire (see Fig. 8b and c).

## 4. Discussion

To validate the values of yield strength generated by various microstructures, we have checked available theoretical and experimental data. Specifically, the yield strengths (16.2–18.8 GPa) of TB- $\text{Ni}_3\text{Al}$  obtained are well consistent with that (14.8–16.8 GPa) of  $\text{Ni}_3\text{Al}$  twinning nanopillars from molecular dynamics simulations [26]. Obviously, these values are smaller than the ideal tensile strength ( $\sim 25.0$  GPa) of  $\text{Ni}_3\text{Al}$  along the [111] orientation according to the first-principle calculation [39]. Here it is worth noting that the first principle can only estimate the upper bound of yield strength without taking temperature, sample size or strain rate into account. We also note that the yield strength (16.9 GPa) of the [111] oriented SC- $\text{Ni}_3\text{Al}$  nanowire is larger than that (10.2 GPa) of  $\text{Ni}_3\text{Al}$  nanocubes with [100] orientation determined from experiments [20]. This is because that the sample size, crystalline orientation and strain rate have significant effects on the yield strength of  $\text{Ni}_3\text{Al}$ . Specifically, Li et al. [40] indicated that the yield strength of dislocation-free  $\text{Ni}_3\text{Al}$  nanocubes increases from  $\sim 2.1$  to  $\sim 4.5$  GPa as the sample size reduces from  $\sim 630$  to  $\sim 180$  nm, with up to 1–2 orders of magnitude higher than that of bulk  $\text{Ni}_3\text{Al}$  [41]. This agrees with the theoretical modeling on the size-dependent yield strength of  $\text{Ni}_3\text{Al}$  micro-pillars [42,43]. In addition, Zhu et al. [44] elucidated that the yield strength at a strain rate of  $10^8 \text{ s}^{-1}$  (corresponding to the scenario of molecular dynamics) is 2–3 times higher than that below a strain rate of  $10^{-2} \text{ s}^{-1}$  (i.e., the experimental results at quasi-static loading conditions).

The simulation results can be further validated by the size and strain rate effects on yield strength and uniform elongation of SC- $\text{Ni}_3\text{Al}$  nanowires. Fig. 9 shows that, as the diameter of nanowires increases from 3 to 12 nm, the yield strength decreases from 19.0 to 16.1 GPa and





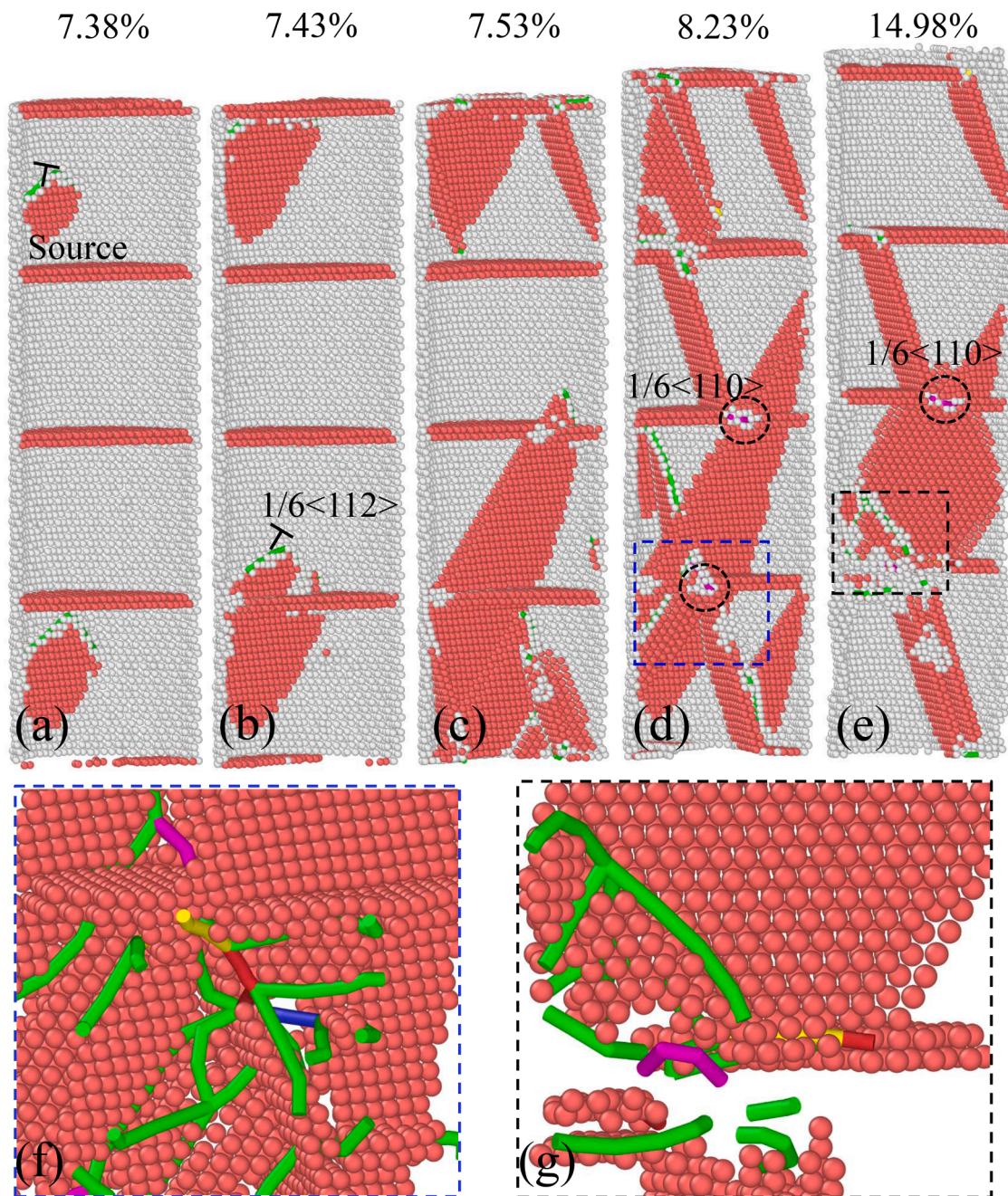
**Fig. 6.** Evolution of microstructures analyzed by the dislocation analysis with strain increasing in a CSF-Ni<sub>3</sub>Al nanowire with a spacing of 4.5 nm between parallel CSFs. (a) a  $1/6\langle 112 \rangle$  Shockley dislocation nucleates on surface of a nanowire and causes fading of CSF (marked by a dashed ellipse) to which it spreads. (b) Motion, nucleation and interaction of  $1/6\langle 112 \rangle$  Shockley with another CSF. (c), (d) and (e) More dislocation activities at various strains. (f) and (g) Local enlarged structures in areas marked by dash boxes in (d) and (e). Structures of dislocations at local regions such as  $1/6\langle 112 \rangle$  Shockley,  $1/6\langle 110 \rangle$  stair-rod and  $1/3\langle 100 \rangle$  Hirth are expressed with green, purple and yellow lines, respectively, and FCC structures are removed for clarity.

the uniform elongation falls from 8.3 to 7.1%. In addition, as the strain rate increases from  $5 \times 10^6$  to  $5 \times 10^{10} \text{ s}^{-1}$ , the yield strength rises from 15.5 to 21.1 GPa and the uniform elongation grows from 6.7 to 11.1% (see Fig. 10). Although there is still a huge difference in comparison with the size and strain rate in experiments, the changing trends are well consistent with experimental observation and theoretical description [41,44]. Hence, taking account of the size and strain rate effects, it is reasonable to conclude that the [111] oriented SC-Ni<sub>3</sub>Al nanowire with a lateral dimension of 6 nm has a yield strength of 16.9 GPa at a strain rate of  $5 \times 10^8 \text{ s}^{-1}$ .

Ductility is usually measured by the uniform elongation or the

elongation to failure [45]. In this work, uniform elongation is employed to characterize ductility because it is not affected by the geometry and size of a sample. As shown in Fig. 8, the uniform elongation and yield strength of nanostructured Ni<sub>3</sub>Al nanowires significantly depend on the type of planar defects. Their deformation mechanisms are attributed to the diversity of interactions between dislocations and planar defects. These interactions produce both profitable and disadvantageous aspects. Profitable factors include impediment of planar defects to propagation of dislocations and pinning of dislocations at a local region. Disadvantages consist of fading of planar defects, detwinning and migration of TBs. In all kinds of nanowires, the first dislocation activity is nucleation





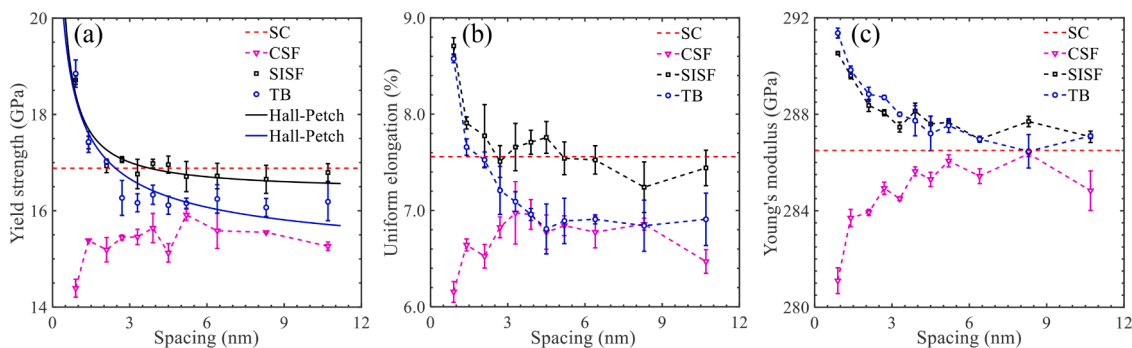
**Fig. 7.** Dislocation activities in an SISF- $\text{Ni}_3\text{Al}$  nanowire under uniaxial tension. Spacing between parallel SISFs is 4.5 nm. (a)  $1/6\langle 112 \rangle$  Shockley dislocations initiate on surface of a nanowire and (b) propagate inward. (c) Dislocations cross over SISFs. (d) and (e) Interaction between  $1/6\langle 112 \rangle$  Shockley dislocations and SISFs brings  $1/6\langle 110 \rangle$  stair-rod dislocations (indicated by dashed circles) which pin dislocations near SISFs. (f) and (g) Local enlarged structures in areas marked by dash boxes in (d) and (e). Microstructural evolution is analyzed by the dislocation analysis, with surface and planar defects being colored in white and red.  $1/6\langle 112 \rangle$  Shockley,  $1/2\langle 110 \rangle$  perfect,  $1/6\langle 110 \rangle$  stair-rod and  $1/3\langle 100 \rangle$  Hirth dislocations are shown with green, blue, purple and yellow lines.

of the  $1/6\langle 112 \rangle$  Shockley dislocation. It accounts for more than 60% density of dislocation lines at an arbitrary strain after its appearance. They can cut through CSFs and SISFs but be stopped by TBs. Interaction between a  $1/6\langle 112 \rangle$  and a CSF induces fading of CSF. Thus, lack of obstacle to propagation of dislocations weakens the yield strength and uniform elongation of CSF- $\text{Ni}_3\text{Al}$  nanowires. On the contrary, in SISF- $\text{Ni}_3\text{Al}$  nanowires, the stability of a  $1/6\langle 110 \rangle$  stair-rod helps to pin dislocations near an SISF, bringing strengthening and toughening. Pinning effect and obstacle of TBs to motion of dislocations are reasons for improvement of yield strength of TB- $\text{Ni}_3\text{Al}$  nanowires. However, detwinning and migration reduce yield strength, declaring the poor performance of TBs to strengthen in comparison with that of SISFs with

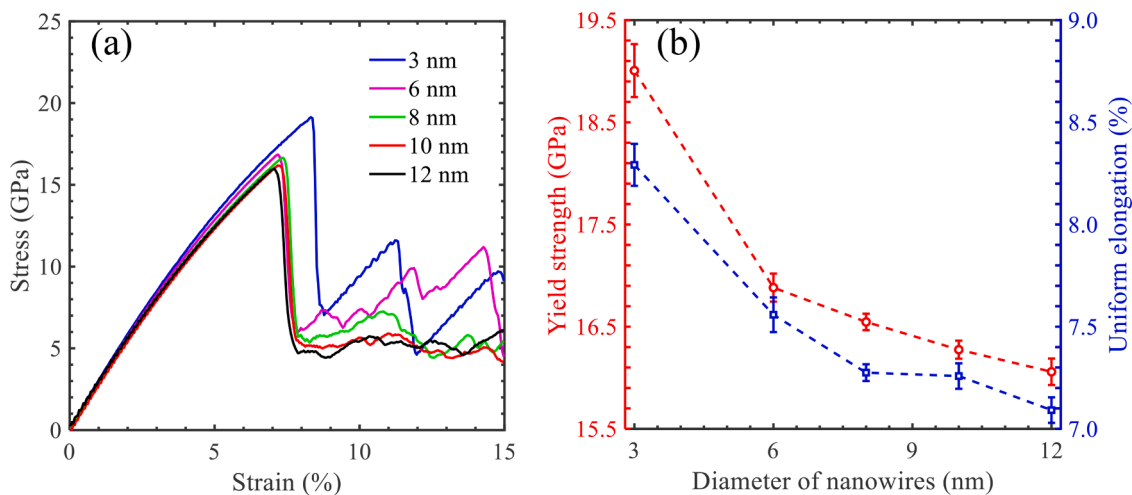
the same spacing between planar defects (see Fig. 8a). Strengthening of both SISFs and TBs can be described by the Hall-Petch relationship, with the exponent of 1 and 1/2, which echo experimental results measured from Mg alloy containing stacking faults [11,12] and nanotwinned copper [8,9,46], respectively.

In addition, it is worth noting that the yield strength sharply decreases with the increase of spacing between TBs (or SISFs) from 0.9 to 3.3 nm. However, there is not a noticeable decrease with further increase of spacing (see Fig. 8a). The similar trends were observed in experiments of Mg alloy with stacking faults and copper with TBs [12,46]. The reason for this is that, the smaller the spacing between planar defects, the more obvious the hindering effect of planar defects to

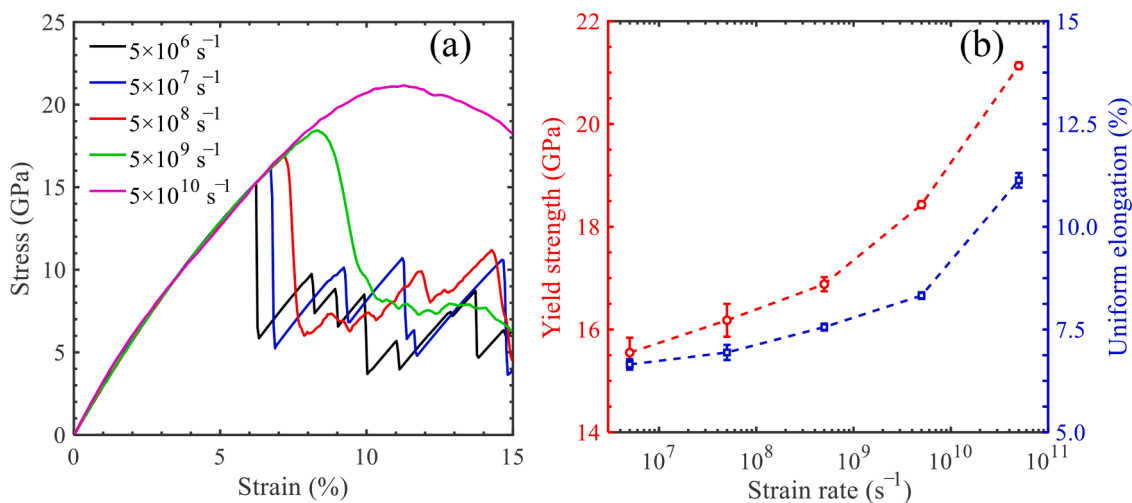




**Fig. 8.** The mechanical properties of nanostructured Ni<sub>3</sub>Al nanowires depend on spacing between planar defects. (a) The yield strength with solid lines fitted by Eq. (3), (b) uniform elongation, and (c) Young's modulus vary with spacing between planar defects.



**Fig. 9.** The sample size effect on the mechanical properties of SC-Ni<sub>3</sub>Al nanowires with a strain rate of  $5 \times 10^8 \text{ s}^{-1}$ . (a) Stress-strain curves and (b) the yield strength and uniform elongation.



**Fig. 10.** The strain rate effect on the mechanical properties of SC-Ni<sub>3</sub>Al nanowires with a diameter of 6 nm. (a) Stress-strain curves and (b) the yield strength and uniform elongation.

dislocation activities is. When the spacing between planar defects is beyond 3.3 nm, the contribution of planar defects to yield strength is inappreciable. This is in agreement with the Hall-Petch relationship. That is, since the variation of yield strength is proportional to  $d^{-(n+1)}$ , the sharply reduced yield strength tends to be stable with the increase of spacing.

The microstructural dependent Young's modulus of Ni<sub>3</sub>Al nanowires is attributed to the energetic stability of CSFs, SISFs and TBs. Based on analysis of first principles, the energy of a CSF is nearly two times over that of an SISF, while an SISF and a TB possess roughly the same energy [26,27,33,47–49]. Since Young's modulus represents the ability of a material to resist elastic deformation, the energetic instability cuts down

such an ability. This leads to a lower Young's modulus of CSF-Ni<sub>3</sub>Al nanowires in contrast to that of SISF- and TB-Ni<sub>3</sub>Al nanowires.

## 5. Conclusion

In summary, a series of molecular dynamics simulations of nanostructured Ni<sub>3</sub>Al nanowires have been performed under uniaxial tension. The mechanical properties and deformation mechanisms of nanostructured Ni<sub>3</sub>Al nanowires have been clarified. It is shown that, the yield strength and uniform elongation of nanostructured Ni<sub>3</sub>Al nanowires significantly depend on the type of planar defects. The different deformation mechanisms are due to the diversity of interactions between dislocations and planar defects. The main conclusions can be summarized as follows:

- (1) In contrast to CSFs, strengthening and toughening can be achieved with SISFs and TBs. The favorable factors are attributed to impediment of planar defects to propagation of dislocations and pinning effect resulting from interaction between dislocations and planar defects. Disadvantageous aspects include fading of planar defects, detwinning and migration of TBs.
- (2) Among these nanowires, SISF-Ni<sub>3</sub>Al nanowires gain the best strengthening and toughening, and CSF-Ni<sub>3</sub>Al nanowires have the worst mechanical properties. Strengthening by SISFs and TBs can be described by the Hall-Petch relationship with an exponent of 1 and 1/2, respectively.
- (3) The Young's modulus of nanostructured Ni<sub>3</sub>Al nanowires depends on their energetic stability of nanostructures. In contrast to SISF- and TB-Ni<sub>3</sub>Al nanowires, CSF-Ni<sub>3</sub>Al nanowires have a lower Young's modulus.

It is expected that these findings could provide new insights into a deep understanding on deformation mechanisms of nanostructured Ni<sub>3</sub>Al and benefit its optimal design and wide application in the aerospace industry.

## CRedit authorship contribution statement

**Zhiwei Zhang:** Conceptualization, Investigation, Methodology, Data curation, Writing – original draft. **Qiang Fu:** Formal analysis. **Jun Wang:** Conceptualization, Supervision, Writing – review & editing, Funding acquisition. **Rong Yang:** Writing – review & editing. **Pan Xiao:** Funding acquisition. **Fujiu Ke:** Conceptualization. **Chunsheng Lu:** Writing – review & editing.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Supplementary materials

Supplementary material associated with this article can be found, in the online version, at doi:10.1016/j.ijmecsci.2021.106953.

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