



Linear correlation between state-of-health and incremental state-of-charge in Li-ion batteries and its application to SoH evaluation

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ABSTRACT

SoH (State-of-Health) evaluation is of pressing need in the health management of commercial Li-ion batteries and has been a topic of intensive research. A simple route to supply a quick, non-destructive, and preferably on-site assessment of SoH with high fidelity is desired. In this paper, analysis based on a partial (dis)charge and a sliding voltage window on the constant-current (dis)charge voltage-time curve may fulfill the need. The incremental State-of-Charge (ΔS_{oc}) (derived from the sliding window) is proportional to the SoH within a suitable voltage region. The slope k of the $S_{oH} - \Delta S_{oc}$ curve and its extrapolated interception at $SoH=1$, denoted as ΔS_{oc}^1 , can then be used to differentiate the remaining life of batteries of the same SoH. The proposed SoH evaluation method, along with the linearity characterized by k and ΔS_{oc}^1 , make it an appealing route toward quick and on-site health management of batteries.

1. Introduction

Li-ion batteries (LIBs) have been extensively used as energy storage systems for portable electronics, electric vehicles, and other fields [1–3]. Immediately after production, LIBs are bound to irreversible degradation, no matter in storage, transportation, in use or lay aside. Quantifying the state of degradation in LIBs is therefore a crucial demand for the economical and reliable operations of LIBs-powered systems [4–8]. The SoH (State-of-Health) is a key parameter evaluating the current working conditions of LIBs. For its self-evident importance, various methods have been proposed to characterize the SoH of LIBs [9–11]. The capacity-fade indicator S_{oH} , defined as the ratio of the current maximum available capacity Q_c to the rated capacity Q_r [11], i.e., $S_{oH} = \frac{Q_c}{Q_r}$, is of general acceptance in the LIBs industry. In fact, in contrast to the simple definition, characterizing the contribution of a particular one out of many mechanisms to the degradation of LIBs (hence SoH) is not an easy job, since the degradation of LIBs often involves multiple interweaving mechanisms and processes [12–17], e.g. active material shedding, loss of electrical contact, lithium loss caused by SEI (Solid–Electrolyte-Interphase) formation, and *etc.* The strong electro-chemo-mechanical coupling behavior during battery degradation [18–22] perplexes the determination of SoH in engineering

applications.

Among different technologies to characterize SoH of LIBs [23–26], two strategies have been prevailing, including a direct measurement and an indirect method [27]. With respect to the direct method, the available capacity and internal resistance are the two critical parameters for battery SoH estimation. The ampere-hour counting method is commonly used to measure available capacity through complete charging and discharging batteries at low current rates [28], which is time-consuming for on-site SoH evaluation. The electrochemical impedance spectroscopy technique, through applying a voltage or current excitation to obtain the change of impedance spectrum, may also reflect the battery degradation [29], which is however subject to data noise and constraints in field test.

Methods through indirect analysis are often either physics- or data-driven-based, and the two also include different variants based on the adopted physical model and the strategy applied for feature extraction. Electrochemical-model-based and equivalent-circuit-model-based methods are the two commonly used physics-based approaches. The electrochemical-model-based approach uses a single physical feature involved in the (dis)charge processes, such as Li-ion concentration [30], SEI film thickness [31], and so on, to extract SoH. As the methods involve coupling of multiple fields, one often needs to solve a group of nonlinear partial differential equations [32,33]. The

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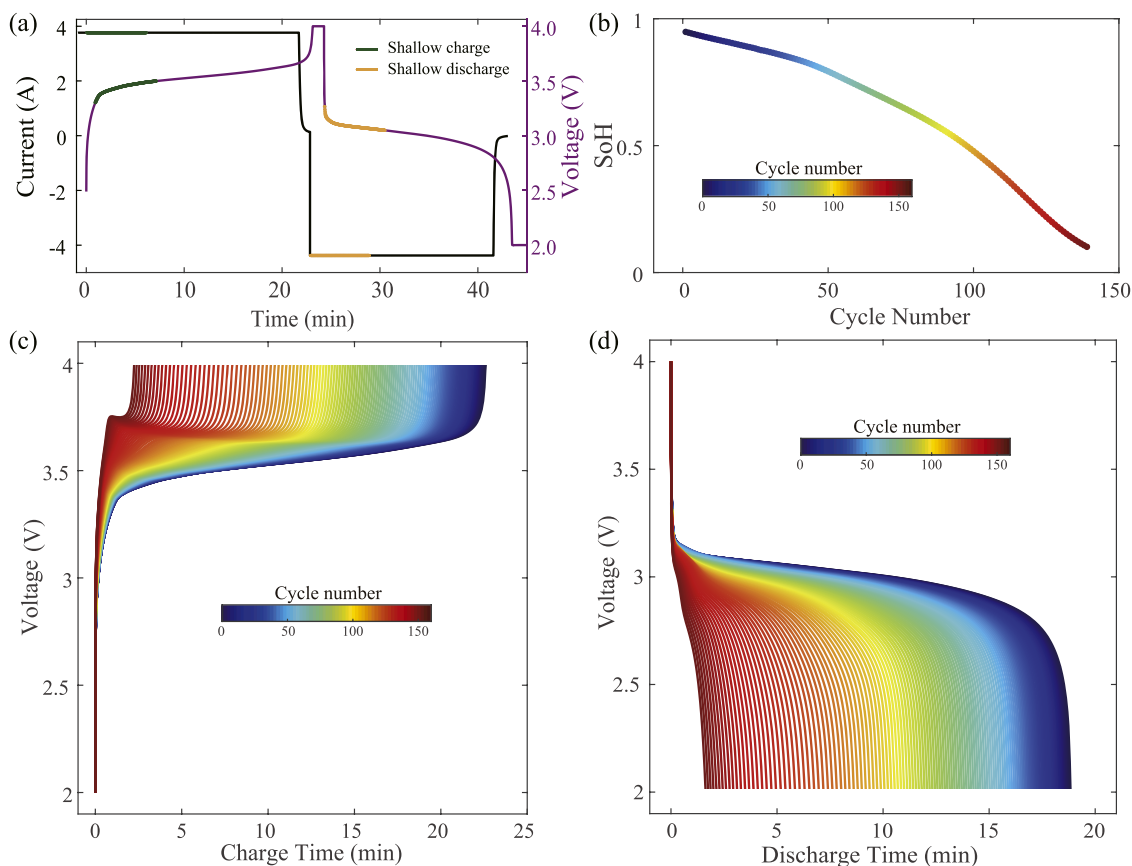


Fig. 1. The evolution of SoH of an LFP/graphite battery. (a) The current-time curve and its corresponding voltage-time response with highlighted shallow CC charge and CC discharge domain in the first full charge-discharge cycle under CC—CV mode (2.5C-3.0D); (b) The SoH vs cycle number curve, in which the color bar denotes cycling history; The voltage-time plots during charging (c) and discharging (d) at different cycles.

equivalent-circuit-model-based methods are of moderate complexity, but limited operating conditions [34].

Data-driven-based methods are sweeping all corners of science, and are also adopted to predict SoH of the energy storage system (such as, battery, supercapacitor, etc.) by extracting essential features from data at hand using either statistical analyses or machine learning techniques [35,36]. Differentiating the contribution of a particular mechanism to capacity degradation and hence to SoH is off the table [37–40]. Both automatic extraction method by deep learning (AEM-DL) framework [41,42] and manual construction based on domain knowledge (MC-DK) framework [43–45] can be utilized for feature extraction. AEM-DL algorithms are usually accompanied with complex computation based on available data, in which the specific meaning of individual features is generally obscure [46,47]. Moreover, the AEM-DL methods use testing data involving a full charging process, from 0% SoC (State-of-Charge) up to 100% SoC at the constant-current constant-voltage (CC—CV) charging mode. To avoid full charging process and reduce the test time, incremental capacity analysis (ICA) methods based on regional capacity and voltage were introduced for SoH estimation [48,49]. However, incremental capacity and differential voltage curves are composed of substantial noise signals and require filtering techniques for data pre-treatment. Besides, the ICA method is restricted to low charge current rates (1/5 to 1/25 C-rate) in order to achieve reasonable fidelity for SoH.

Owing to the rapid development of novel data-driven-based methods, many endeavors have been devoted to effective feature extraction for SoH [50–52]. Liu et al. [53,54] estimated SoH with GPR (Gaussian Process Regression) and RVM (Relevance Vector Machine), and such methods can provide the posterior probability of predictions. Li et al. [55] applied transfer learning and network pruning to establish compact convolutional neural network models to improve the accuracy

of SoH estimation. Regardless of the tremendous successes, differentiating battery-wise distinctions in SoH using data-driven methods remains challenging. The reliability depends highly on the data characteristics and volume [56]. High computational cost is another issue to prevent its application from on-site application [57].

In this report, we propose a quick, non-destructive, and potentially on-site assessment of SoH with high fidelity, and discuss its implication for differentiating the performance of batteries. We introduce in the second section the data acquisition details, followed with the sliding voltage window strategy to construct the SoH evaluation in Section 3, and report a linear relationship between SoH and the increment SoC. In Section 4 we demonstrate how the slope k of the $S_{oH} - \Delta S_{oC}$ curve and its interception at $S_{oH}=1$ (ΔS_{oC}^1) can be adopted to make a distinction about the remaining life of the batteries of same SoH. We conclude in Section 5 with further discussions on the implications of the methods for the health management of batteries.

2. Experimental section

The experiments were performed on commercial LFP (LiFePO₄)/graphite batteries (LISHEN, 18,650 cylindrical battery, 1.5 Ah nominal capacity). The LFP/graphite batteries were cycled by NEWARE battery testing systems with a sampling frequency of 1 Hz at 25 °C in a temperature-controlled environmental chamber. Typical constant-current constant-voltage (CC—CV) charging and discharging profiles adopted for the cycling measurements are shown in Fig. 1a. The cut-off voltage in constant-current (CC) charging stage and CC discharging stage are set to 4.0 and 2.0 V, respectively. The cut-off current during constant-voltage (CV) stage is set to 0.05C, where 1C is equal to 1.5 A. A dataset including 48 LIBs was generated, including 6 groups and each

Table 1

The charge-discharge settings of the six groups of LIBs. In each group, there are eight batteries which were tested with the same charge and discharge profile listed here.

Group No.	Charge-Discharge Profiles	Abbreviations
1	1.0C charge – 3.0C discharge	1.0C-3.0D
2	1.5C charge – 3.0C discharge	1.5C-3.0D
3	2.0C charge – 3.0C discharge	2.0C-3.0D
4	2.5C charge – 3.0C discharge	2.5C-3.0D
5	2.0C charge – 2.0C discharge	2.0C-3.0D
6	2.5C charge – 2.5C discharge	2.5C-2.5D

applied with the same charge and discharge profile. The 6 charge-discharge profiles are set with different CC (dis)charge rates, what are detailed in Table 1.

With the CC–CV charge and discharge (2.5C-3.0D) applied to an LFP/graphite battery, the current-time curve in the first cycle is what we see in Fig. 1a. With cycling proceeding, the delivered capacity exhibits an apparent decay (see Fig. 1b), suggesting the SoH degradation. Extracting the corresponding voltage-time curves from the charge (Fig. 1c) and discharge (Fig. 1d) at different cycles, it can be seen that the time in the CC charge and CC discharge stages are greatly shortened

with cycling, indicating a more prominent voltage-changing (discharging) rate at higher cycle numbers.

3. Modelling

Fig. 1 shows the response of a battery subject to full CC–CV charge and discharge cycle. We are interested in utilizing the voltage change in time during CC charge and CC discharge stages, and proceed to show how we may evaluate SoH from the voltage-time curves during both CC charging and CC discharging processes but with a shallow (dis)charging strategy, as illustrated in Fig. 1a.

3.1. S_{oH} - ΔS_{oC} evolution during discharging

To depict the SoH degradation from the voltage-time curves at CC discharge stages, we examine the variation of time Δt (equivalently ΔS_{oC} through $\Delta S_{oC} = C\Delta t$ where C means (dis)charge rate in the CC stage) for a given voltage drop (ΔV) in the voltage-time curves at different cycles, as illustrated in Fig. 2a. One may think of different ways to determine the starting voltage V_s in a discharge curve. We adopt a correlation analysis based on the spearman coefficient ρ [58] to indicate the statistical dependence of SoH on ΔS_{oC} for a variety of combinations of ΔV

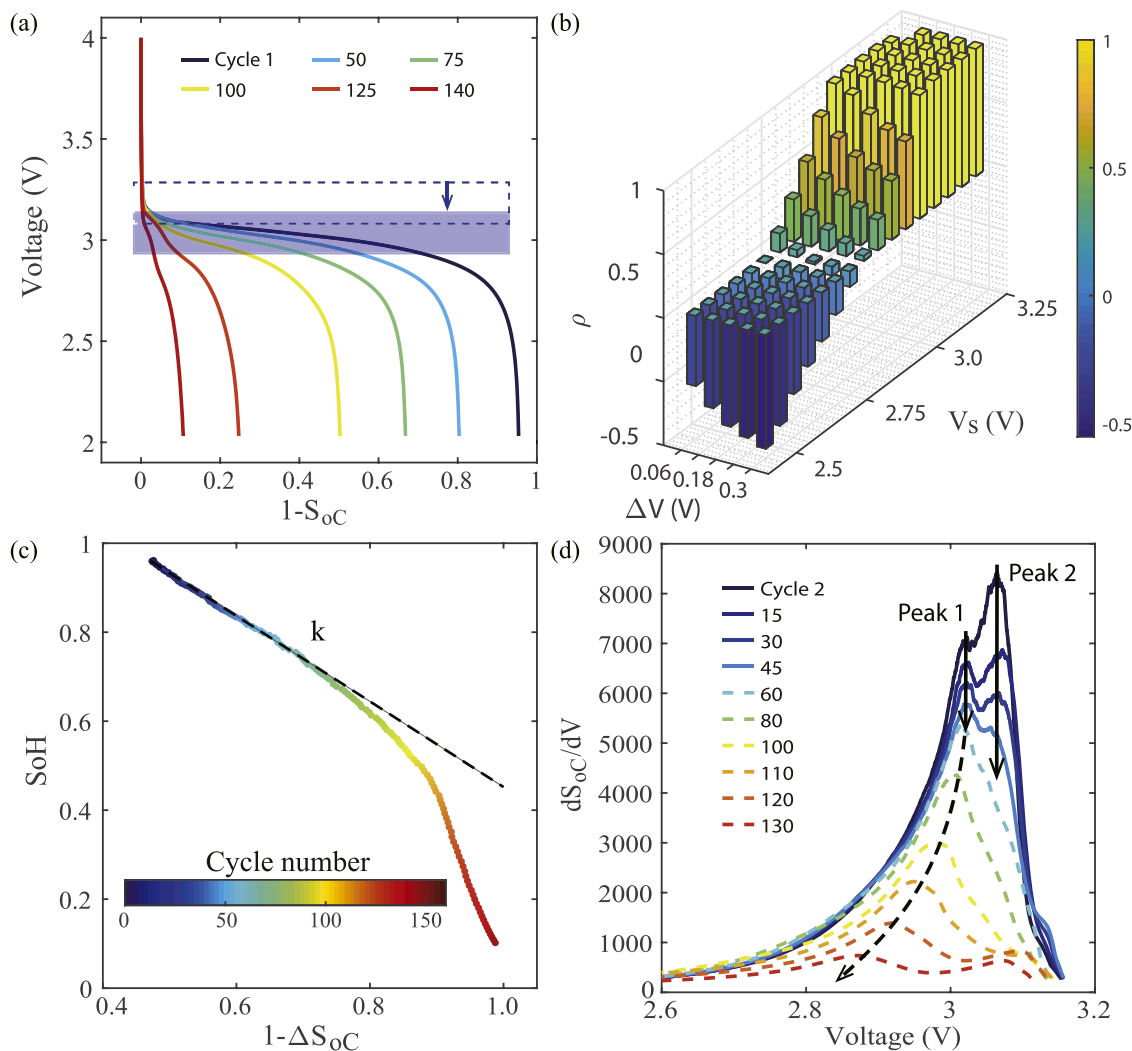


Fig. 2. The S_{oH} - ΔS_{oC} evolution rule during discharging in the total cycle-life of the batteries, cycled with CC–CV mode (2.5C-3.0D). (a) The voltage-($1-S_{oC}$) plots during the 3C CC discharge stages at different indicated cycles. The light blue color region marks the selected voltage window for S_{oH} - ΔS_{oC} correlation analysis; (b) The spearman correlation coefficient image between SoH and ΔS_{oC} with different voltage window (ΔV , V_s); (c) The SoH-($1-\Delta S_{oC}$) plots using the voltage window $\Delta V = 0.3$, $V_s = 3.3$; (d) The dS_{oC}/dV -voltage curves at different cycles.

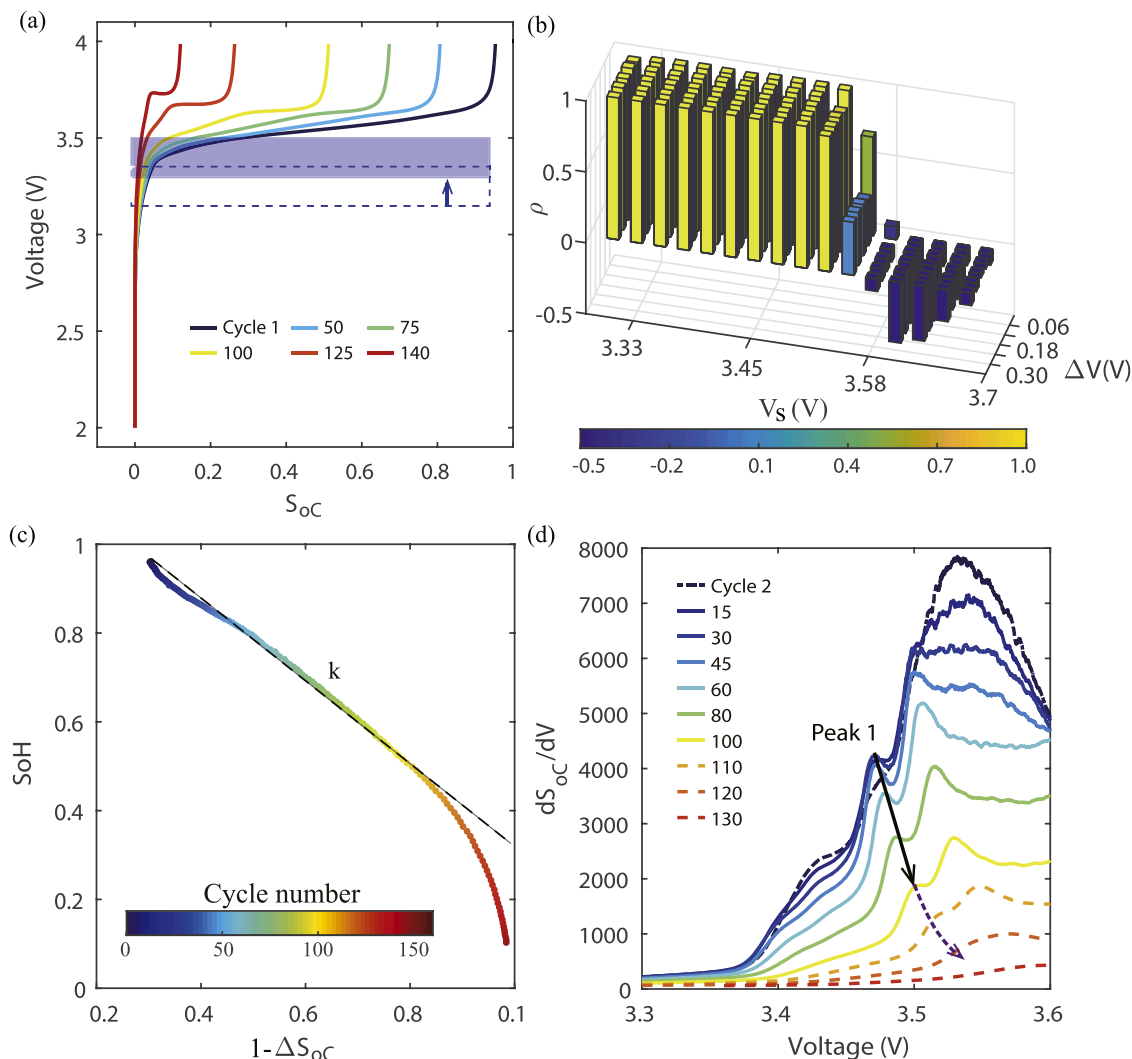


Fig. 3. The $S_{oH}-\Delta S_{oC}$ evolution rule at the charge stage in the total life cycle of the batteries, cycled with CC–CV mode (2.5C–3.0D). (a) The voltage- S_{oC} evolution curve during the 2.5C CC charge stages at different indicated cycles; (b) The spearman correlation coefficient image between SoH and ΔS_{oC} with different ($\Delta V, V_s$) conditions; (c) The SoH-($1-\Delta S_{oC}$) correlation plot with the voltage window ($\Delta V = 0.3, V_s = 3.3$); (d) The dS_{oC}/dV -voltage curves at different cycles.

and V_s . As seen from Fig. 2a, for each V_s and ΔV , the ΔS_{oC} can be read at the voltage ($\Delta V, V_s$). We have S_{oHj} and ΔS_{oCj} from a voltage-time curve at the j -th cycle. After converting (ΔS_{oCj}) and (S_{oHj}) to ranks $R(\Delta S_{oCj})$ and $R(S_{oHj})$, we define d_j the difference between the two ranks, $d_j = R(\Delta S_{oCj}) - R(S_{oHj})$. The Spearman correlation coefficient ρ can be computed using the formula below

$$\rho = 1 - \frac{6 \sum_{j=1}^n (d_j)^2}{n(n^2 - 1)}, \quad (1)$$

where n is the total number of cycles, which is battery-specific. Note that ρ ranges from -1 to 1 , where $\rho = 1, 0$, and -1 indicate a perfect positive association of ranks, no association of ranks, and a perfect negative association between ranks, respectively.

The correlation between SoH and ΔS_{oC} , with different voltage windows ($\Delta V, V_s$) from the voltage-($1-S_{oC}$) curve at the 3C CC discharge rate, is then examined. As seen in Fig. 2b, a strong positive association between SoH and ΔS_{oC} is found at the initial discharging process (3.2 to 2.9 V). As the selected voltage window slides down to lower voltages, the correlation reduces and disappears (ρ becomes negative as the voltage drops from 2.9 to 2.5 V). Taking the sliding voltage window $\Delta V = 0.3, V_s = 3.3$ as an example, see the S_{oH} -($1-\Delta S_{oC}$) curve in Fig. 2c, a strong correlation is indicated between SoH and ΔS_{oC} : SoH firstly

decreases proportionally with decreasing ΔS_{oC} at the initial degradation stage, and then followed by a nonlinear degradation as ΔS_{oC} reduces further.

The incremental capacity (IC) curve, calculated as the derivative of S_{oC} with respect to voltage (dS_{oC}/dV vs. V), is commonly applied to reveal characteristic peaks associated with different chemical reaction processes. The peak features in IC curves, including the amplitude, area, and peak shifts, may change with battery cycling, which can be applied for SoH analyses [49]. Fig. 2d shows the IC curves at different cycles extracted from the tested voltage vs. ($1-S_{oC}$) curves (Fig. 2a). Often there are two peaks on the IC curves at an early degradation stage (marked by the solid black arrow in Fig. 2d), and the intensity of the two peaks decay with cycling. At this stage, there is a strong linear correlation between SoH and $1-\Delta S_{oC}$, as demonstrated in Fig. 2c. Further cycling leads to accelerated degradation, as exemplified by the significant intensity decay and position offset of Peak 1 to the lower end voltage (marked by the dashed black arrow in Fig. 2d). Peak 2 becomes invisible at this stage. The accelerated degradation regime on IC curves in Fig. 2d refers perfectly to the nonlinear $S_{oH}-\Delta S_{oC}$ evolution period shown in Fig. 2c.

3.2. $S_{oH}-\Delta S_{oC}$ evolution during charging

The $S_{oH}-\Delta S_{oC}$ correlation is also present at the CC charge stages, as

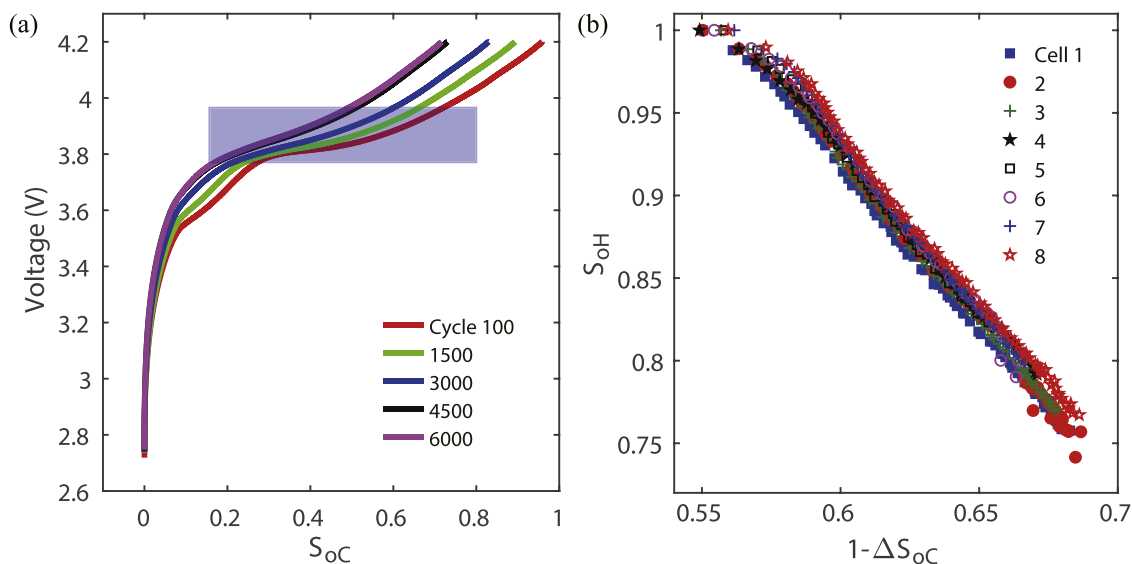


Fig. 4. Validation of the $S_{oH}-\Delta S_{oC}$ model during CC charging by the pouch LIBs. The exploited dataset includes eight Kokam pouch batteries from Birkel et al. [59, 60]. (a) The voltage- S_{oC} evolution curves during the 1C CC charge stages at different cycles; (b) The $S_{oH}-(1-\Delta S_{oC})$ relationship with the sliding voltage window ($\Delta V = 0.2, V_s = 3.8$) at the 1C charge rate. .

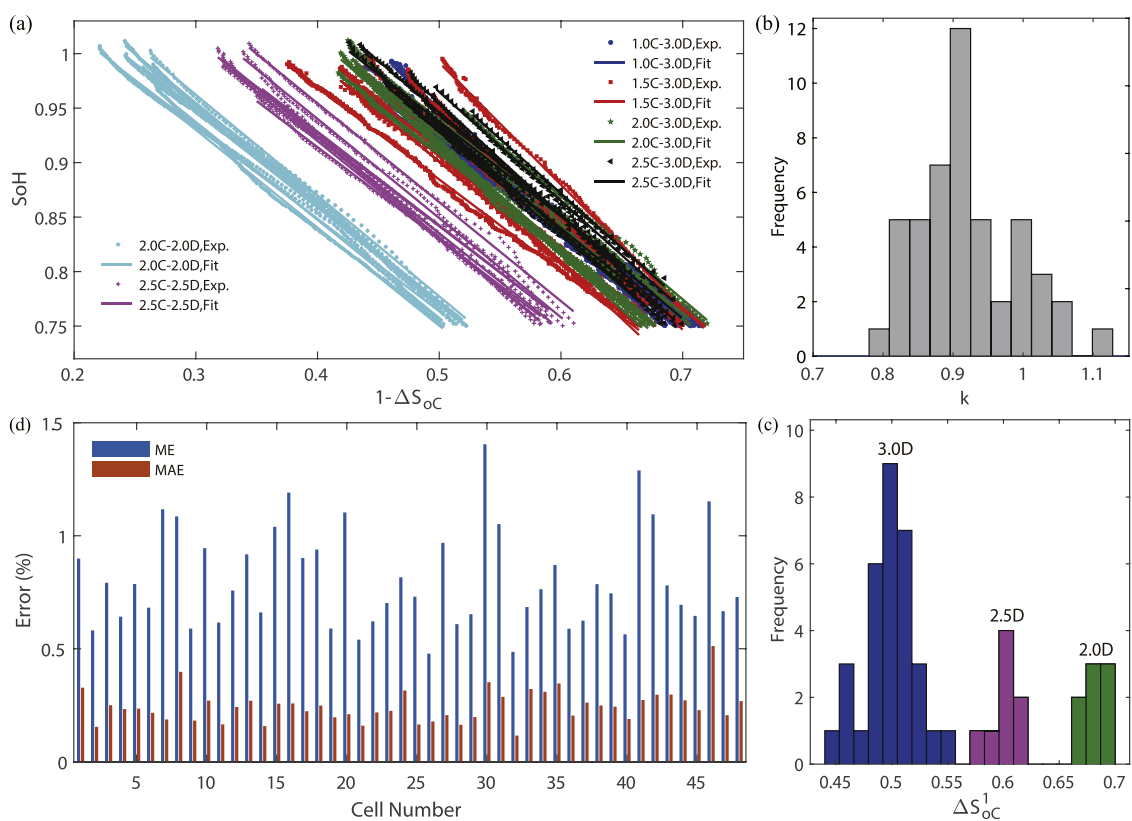


Fig. 5. The linear $S_{oH}-\Delta S_{oC}$ evolution. (a) The linear $S_{oH}-\Delta S_{oC}$ evolution of LIBs with different CC charge and CC discharge rates (Markers: experimental results; Solid lines: fitting results). Distributions of (b) k and (c) ΔS_{oC}^1 from linear fitting results. (d) The fitting errors of each battery in a dataset of 48 batteries are examined.

shown in Fig. 3. By choosing a voltage window (the light blue color marked region in Fig. 3a) and sliding along the voltage-time curves from low voltage to high voltage, we show in Fig. 3b the Spearman coefficient ρ between S_{oH} with ΔS_{oC} . A strong correlation is indicated at the initial charge stage with low voltages. Fig. 3c shows the $S_{oH}-\Delta S_{oC}$ relationship with a suitable voltage window of $\Delta V = 0.3, V_s = 3.3$, a linear evolution is observed for S_{oH} to 0.5. In the linear $S_{oH}-\Delta S_{oC}$ evolution stage, Peak 1

shows an intensity reduction and position offset to the higher voltage end (marked by the solid black arrow in Fig. 3d). Progressive decay in S_{oH} , as seen in Fig. 3c, may be identified by the leveled-out intensity Peak 1, as indicated by the dashed blue arrow in Fig. 3d.

Our sliding voltage window method is further validated with another experimental dataset of 8 Kokam pouch batteries (SLPB 533459H, 0.74Ah nominal capacity) with a mixed positive electrode of lithium

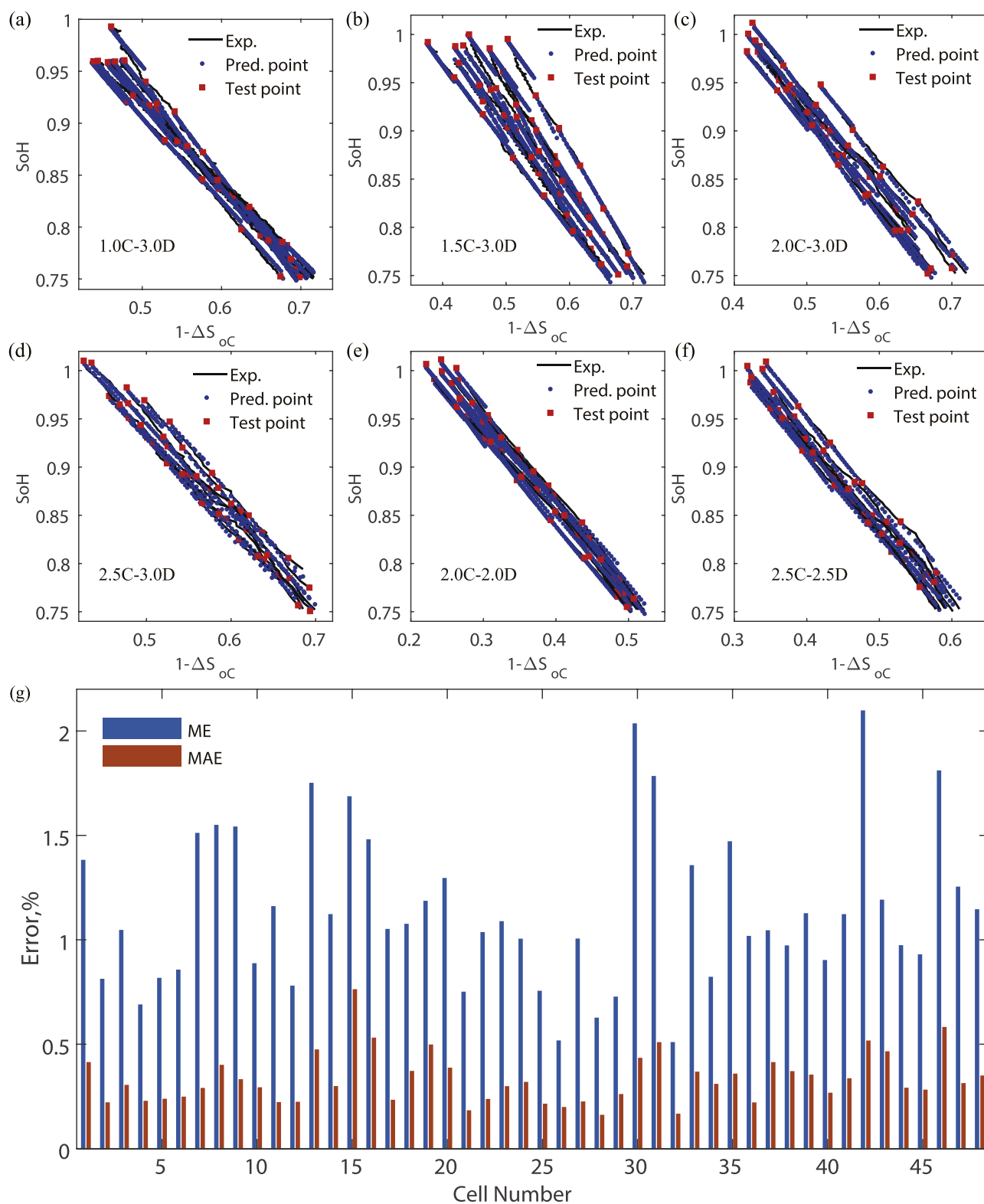


Fig. 6. Application by utilizing the linearity of $S_{oH}-\Delta S_{oc}$ for SoH prediction. (a-f) The linear $S_{oH}-\Delta S_{oc}$ evolution of LIBs with different charge and discharge rates (blue points: predicted SoH evolution; black solid lines: experimental results; red points: certain test points from experiments). (g) The errors of our prediction errors for the 48 batteries.

cobalt oxide and lithium nickel cobalt oxide, and graphite as negative electrode material [59,60]. The pouch batteries were cycled with two different types of charge and discharge profiles (the dynamic-driving-profile and the characterization cycles) at 40 °C. The dynamic-driving-profile is composed of a 2C (1C corresponds to 0.74 A)

CC charge and the Artemis urban drive cycle with an average discharge current of 1.36 A [61]. After each 100 dynamic-driving-profile cycles, a characterization cycle is then employed with the 1C CC charge and discharge. Fig. 4a shows the voltage- S_{oc} curves during charging at different characterization cycles. For the $S_{oH}-(1-\Delta S_{oc})$ correlation

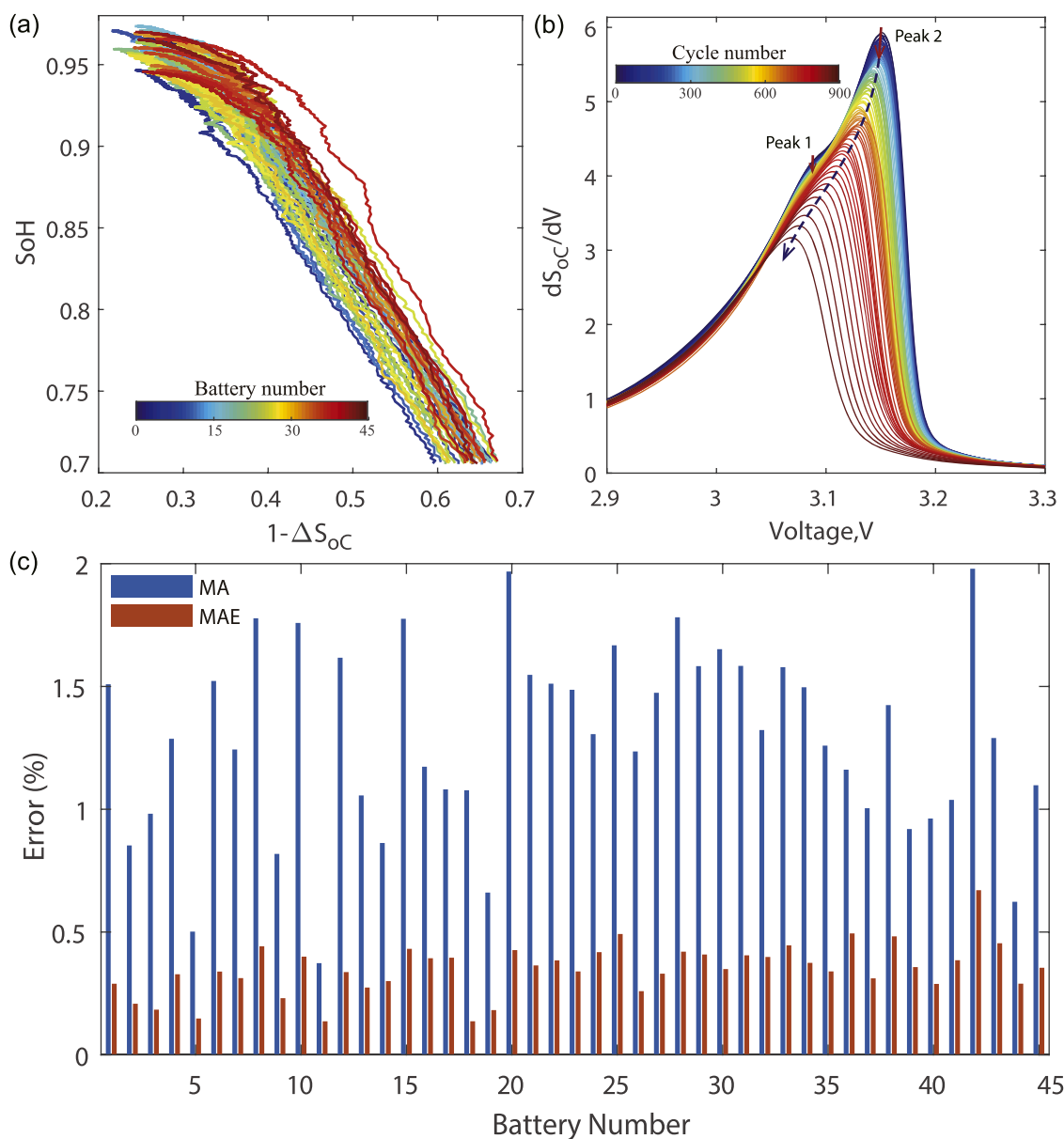


Fig. 7. Validation of the $S_{oH}-\Delta S_{oC}$ linearity from the 4C CC discharge stages in a dataset including 45 A123 LFP/graphite batteries from Attia et al. [63]. (a) The $S_{oH}-(1-\Delta S_{oC})$ plots with the voltage window ($\Delta V = 0.3, V_s = 3.3$). (b) The dS_{oC}/dV -voltage curves at different cycles from one battery of the indicated dataset. (c) The fitting error on SoH of each battery in comparison with the extracted one from the linear $S_{oH}-\Delta S_{oC}$ relationship.

evaluation, a voltage window ($\Delta V = 0.2, V_s = 3.8$), in the 1C CC charge stage (light blue color marked region in Fig. 4a), is employed. We show in Fig. 4b the $S_{oH}-(1-\Delta S_{oC})$ evolution curves of the 8 Kokam batteries. The $S_{oH}-(1-\Delta S_{oC})$ evolution pattern is in concerted with what we demonstrated in Figs. 2c and 3c.

3.3. Linear $S_{oH}-\Delta S_{oC}$ relationship

A total of 48 LISHEN LFP/graphite LIBs with 6 different charge-discharge rates are then employed for cycling performance check. The linear evolution stage of the $S_{oH}-\Delta S_{oC}$ relationship is then extracted from voltage-time curves at CC discharge stages. The cut-off condition of the linear $S_{oH}-\Delta S_{oC}$ evolution rule is set to an offset voltage of Peak 1 of 0.3% in IC curves, deviating from the initial voltage position. The extracted linear $S_{oH}-\Delta S_{oC}$ evolution stage of the total 48 batteries falls primarily within the region $S_{oH} > 0.75$ (Fig. 5a), which is the typical working condition as the first-life of LIBs with high reliability [62]. We then define the linear $S_{oH}-\Delta S_{oC}$ relationship as

$$S_{oH} = 1 + k(\Delta S_{oC} - \Delta S_{oC}^1), \quad (2)$$

where k reflects the degradation slope and ΔS_{oC}^1 is the extrapolated interception at $S_{oH} = 1$.

The $S_{oH}-\Delta S_{oC}$ curves from a broad variety of charging rates, as seen in Fig. 5a, suggest the robustness of the linear degradation characterized by k and ΔS_{oC}^1 . The histograms of k and ΔS_{oC}^1 are shown in Fig. 5b and Fig. 5c, respectively. It can be seen that the slope k is insensitive to the CC charge and CC discharge rates, at least within our exploration with 48 cells. The trend of ΔS_{oC}^1 is evident, it increases as decreasing discharge rate, as shown in Fig. 5c.

The linearity of $S_{oH}-\Delta S_{oC}$ is crucial to the SoH estimation. We now demonstrate that this feature can be utilized to assess SoH by adopting shallow (dis)charging. We define both commonly used error criteria to evaluate the linearity as the Maximum Error (ME), $ME = \max_{i=1,2,\dots,n} (y_i - \hat{y}_i)$ and the Mean Absolute Error (MAE), $MAE = \frac{1}{n} \sum_{i=1}^n |y_i - \hat{y}_i|$. Here y_i and

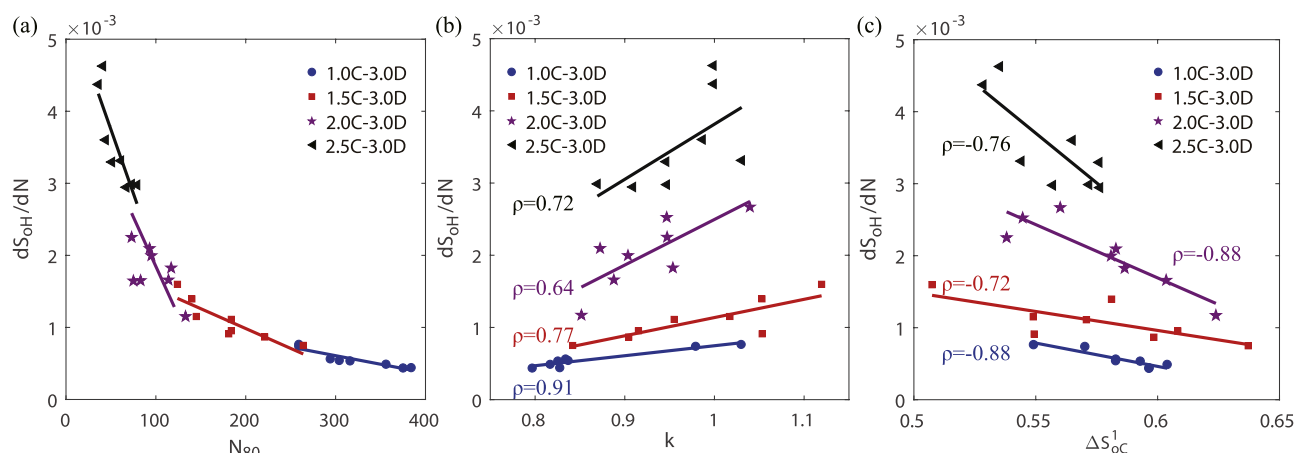


Fig. 8. The correlation analyses between linear $S_{oH}-\Delta S_{oC}$ evolution performance and cycle-life of the 32 LISHEH LFP/graphite batteries. (a) The $dS_{oH}/dN-N_{80}$ (N_{80} : total cycle number till SoH descending to 0.8), (b) $dS_{oH}/dN-k$ and (c) $dS_{oH}/dN-\Delta S_{oC}^1$ plots under charge rates 1.0C, 1.5C, 2.0C, and 2.5C, but the same 3C discharge rate. (Symbols: experimental data; Solid lines: linear fitting).

\hat{y}_i are observed and fitted SoH, respectively, and n is the total number of the tested SoH. The fitting errors of 48 batteries are shown in Fig. 5d. We can see that the fitted MEs of SoH range from 0.4% to 1.4% in the 48 batteries, and the MAEs are smaller by 0.5%.

We then predicted the SoH evolution of the 48 batteries based on k and ΔS_{oC}^1 . Fig. 6a-f show the comparison between experimentally measured (black solid lines) and predicted SoH (blue points). For the SoH prediction, accompanied with a drop of SoH up to 0.04 (red points), the k value was then corrected once to improve accuracy. In engineering practice, for example in electrical vehicles, the parameter correction process can be performed during the annual maintenance of vehicles. The predictability of our model for the 48 batteries is shown in Fig. 6g. We can see that the ME of SoH ranges from 0.5% to 2% in the 48 batteries, and the MAE is within 0.7%, which are comparable to fitting results shown in Fig. 5d. The efficacy of the model demonstrated through Fig. 6 highlights the robust predictability when employing the linear $S_{oH}-\Delta S_{oC}$ relationship for SoH estimation.

We further validated the $S_{oH}-\Delta S_{oC}$ linearity by another dataset of a total 45 LIBs [63] with the LFP cathode and the graphite anode (A123, 1.1Ah nominal capacity). The 45 A123 LIBs were cycled with the same discharging profiles using 4C (1C=1.1A) CC discharge rate till 2 V CV mode with a 1/50C cut-off current. We show in Fig. 7 the $S_{oH}-\Delta S_{oC}$ evolution by applying the voltage window ($\Delta V = 0.3$, $V_s = 3.3$) to the 4C discharge voltage-time curve. A strong correlation between SoH and ΔS_{oC} can also be found in Fig. 7a. Different from the $S_{oH}-\Delta S_{oC}$ relationship shown in Fig. 2c (LISHEH LFP/graphite batteries), a nonlinear evolution occurs in the initial stage, predominantly when $SoH > 0.93$, and followed by a linear evolution until $SoH = 0.7$. Two different evolution stages from the IC curves are shown in Fig. 7b: for the two peaks shown in the IC curves, and the intensity of peak 1 reduces at the initial nonlinear stage and disappears by the end. In contrast, the magnitude of Peak 2 drops proportionally with cycling in the linear $SoH-\Delta S_{oC}$ region. The linearity of the evolution stage is then examined for each battery in the dataset composing 45 A123 batteries (Fig. 7c). The fitted ME of SoH ranges from 0.4% to 2.0%, and the MAE is smaller by 0.5%. The ME, based on SoH measured against SOH predicted, ranges from 0.4% to 2% in the 48 batteries, and the MAE is even smaller and within 0.7%. In comparison with the error results from other SoH estimation models [25], the proposed model can give more competitive SoH estimation on accuracy. Applications of our model to data from two independent studies (Figs. 5 and 7) indicate its efficiency and capability for generalization.

4. Cycle-life property evaluated by the linear $S_{oH}-\Delta S_{oC}$ indexes

We analyze the correlation between the linear $S_{oH}-\Delta S_{oC}$ evolution and the cycle life of batteries. A total of 32 LISHEH LFP/graphite batteries with the same 3C discharge rate (constant current) and four different charge rates (Groups 1 to 4 described in Table 1) are employed to extract the linear $S_{oH}-\Delta S_{oC}$ evolution (see Fig. 5a). The average degradation rate of SoH, defined by dS_{oH}/dN , may then serve the purpose of indicating cycle-life property of LIBs. Since the linear $SoH-\Delta S_{oC}$ evolution of LIBs is within their serving status of high reliability, e.g., for electric vehicle batteries, $SoH > 0.8$, we show in Fig. 8a the correlation between dS_{oH}/dN and the cycle-life N_{80} – the cycle number till SoH degrades to 0.8. The tight negative correlation between dS_{oH}/dN and N_{80} indicates that the batteries with the lower dS_{oH}/dN would exhibit better cycle-life properties.

The correlations of dS_{oH}/dN with k and ΔS_{oC}^1 are shown in Fig. 8b and 8c, respectively. The dS_{oH}/dN vs. k plots, shown in Fig. 8b, indicate positive correlation for the same (dis)charging profile. In particular, the strongest positive correlation between dS_{oH}/dN and k in Fig. 8b occurs when 1.0C charge rate was applied, where its degradation rate of SoH is the lowest among the four (dis)charging profiles investigated here. We then check the correlation between dS_{oH}/dN and the extrapolated interception ΔS_{oC}^1 . The correlation between dS_{oH}/dN and ΔS_{oC}^1 is shown in Fig. 8c, indicating a negative correlation. Results shown in Fig. 8 then suggest that the batteries with lower k and greater ΔS_{oC}^1 would have better cycling performance. As a corollary, both k and ΔS_{oC}^1 may be adopted as auxiliary parameters, in addition to S_{oH} , to further differentiate the remaining life of batteries with close SoH.

5. Conclusion

Through experimental investigations and theoretical analyses by taking a sliding voltage window in the constant-current (dis)charge voltage-time curve of LIBs, we explored the correlation between SoH and the incremental SoC (ΔS_{oC}): In commonly reliable SoH operation, the ΔS_{oC} and the SoH follow a linear relationship within a suitable voltage region. The linearity of $S_{oH}-\Delta S_{oC}$ is also validated through experiments with different battery types and manufacturers, and source data from different groups. Such a linearity between $S_{oH}-\Delta S_{oC}$, as characterized by two core indexes (the slope k and the extrapolated interception ΔS_{oC}^1), can then be employed to estimate the SoH of LIBs during onward cycling, by adopting shallow (dis)charge.

By virtue of the linearity between $S_{oH}-\Delta S_{oC}$, we may acquire sequential evaluation for SoH of LIBs in onward cycling by adopting

shallow (dis)charge. In comparison with existing proposals to characterize SoH of LIBs [23–27], we find the following features makes this proposal a distinct one: (1) Our strategy of estimating SoH is applicable to both the commonly applied CC charge and CC discharge profiles in engineering, with no restriction to (dis)charging rates; (2) The method is simple and easy to be implemented since the input is voltage – time curve at even shallow (dis)charging; (3) The method is robust in terms of efficacy and accuracy for SoH evaluation regardless of the quality of voltage – time curve, which makes the method fit to quick assessment, in less than a few minutes.

In conclusion, we report in this paper a practicable SoH estimation model for LIBs, which after the initial two to three full cycles of charge-discharge, we may evaluate with high fidelity the SoH based on partial charge and discharge segment method. The proposed SoH estimation is quick and non-destructive, and could be applied to monitor the health of commercial LIBs in service.

Credit author statement

Y. Wei conceived the project; J. Wen and Q. Zou did the data analysis; C. Chen performed the experiments. All authors involved in paper writing, data analysis and discussion.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data availability

Data will be made available on request.

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